

ROLLOVER PROTECTIVE STRUCTURES (ROPS) FOR WHEELED AGRICULTURAL TRACTORS

Foreword—This Reaffirmed Document has been changed only to reflect the new SAE Technical Standards Board format. Definitions have been changed to Section 3. All other section numbers have changed accordingly.

1. Scope

1.1 Fulfillment of the intended purpose requires testing as follows:

1.1.1 A laboratory test, under repeatable and controlled loading, to permit analysis of the ROPS for compliance with the performance requirements of this SAE Standard. Either the static test (6.1) or the dynamic test (6.2) shall be conducted.

1.1.2 A crush test to verify the effectiveness of the deformed ROPS in supporting the tractor in an upset attitude.

1.1.3 A field upset test under reasonably controlled conditions, both to the rear and side, to verify the effectiveness of the protective system under actual dynamic conditions. (See 6.4.1.1 for requirements for the omission of this test).

1.1.4 In addition to the laboratory and field loading requirements, there is a temperature-material requirement. (See 7.1.2.)

1.2 The test procedures and performance requirements outlined in this document are based on currently available engineering data.

1.3 Purpose—The purpose of this document is to establish the test and performance requirements of a rollover protective structure (ROPS) designed for wheel-type agricultural tractors to minimize the frequency and severity of operator injury resulting from accidental upsets. All self-propelled implements are excluded.

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2. References

2.1 Applicable Publications—The following publications form a part of the specification to the extent specified herein. Unless otherwise indicated, the latest revision of SAE publications shall apply.

2.1.1 SAE PUBLICATIONS—Available from SAE, 400 Commonwealth Drive, Warrendale, PA 15096-0001.

SAE J114—Seat Belt Assembly Webbing Abrasion Performance Requirements
SAE J117—Cancelled in 1993
SAE J140—Seat Belt Hardware Test Procedure
SAE J141—Seat Belt Hardware Performance Requirements
SAE J339—Seat Belt Assembly Webbing Abrasion Test Procedure
SAE J429—Mechanical and Material Requirements for Externally Threaded Fasteners
SAE J674—Safety Glazing Materials—Motor Vehicles
SAE J800—Motor Vehicle Seat Belt Assembly Installations
SAE J995—Mechanical and Material Requirements for Steel Nuts
SAE J1349—Engine Power Test Code—Spark Ignition and Compression Ignition—Net Power Rating

2.1.2 ASTM PUBLICATION—Available from ASTM, 100 Barr Harbor Drive, West Conshohocken, PA 19428-2959.

ASTM A 370-76—Standard Methods and Definitions for Mechanical Testing of Steel Products

3. Definitions

3.1 Agricultural Tractor—An Agricultural Tractor, for purposes of this document, is defined as a 2- or 4-wheel-drive type machine of more than 15 kW (20 hp) net engine power as defined by SAE J1349, designed primarily to provide the tractive power to pull, push, carry, propel, and/or provide power to implements designed primarily for agricultural usage.

3.2 Tractor Mass—The Tractor Mass is defined as the maximum gross machine mass determined by the manufacturer or a minimum ratio of mass-to-maximum power takeoff power at rated engine speed of 67 kg/kW (110 lb/hp), whichever is greater. The mass includes the ROPS, all fuels, and other components required for normal use. (In case power takeoff power is not available, use 95% of net engine flywheel power.)

3.3 Rollover Protective Structure—A Rollover Protective Structure (ROPS) is a cab or frame for the protection of operators of agricultural wheeled tractors to minimize the possibility of serious operator injury resulting from accidental upsets. The protective structure is characterized by providing space for the clearance zone inside the envelope of the structure or within a space bounded by a series of straight lines from the outer edge of the structure to any part of the tractor that might come in contact with flat ground, and is capable of supporting the tractor in that position if the tractor overturns. (See Figures 1, 2, and 3 for typical configurations.)

3.3.1 SEAT REFERENCE POINT¹—(SRP in Figures 4, 5, and 6) is that point where the vertical line tangent to the most forward point at the longitudinal seat centerline of the seat back, and the horizontal line tangent to the highest point of the seat cushion intersect in the longitudinal seat centerline section. The SRP is determined with the seat unloaded and adjusted to the highest and most rearward position provided for seated operation of the tractor.

1. Consideration is being given to adopting the ISO definition when it is approved.

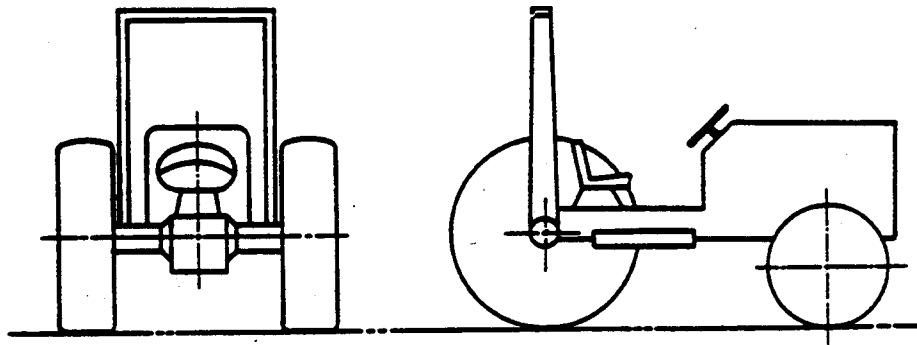


FIGURE 1—TRACTOR WITH TYPICAL TWO-POST ROPS

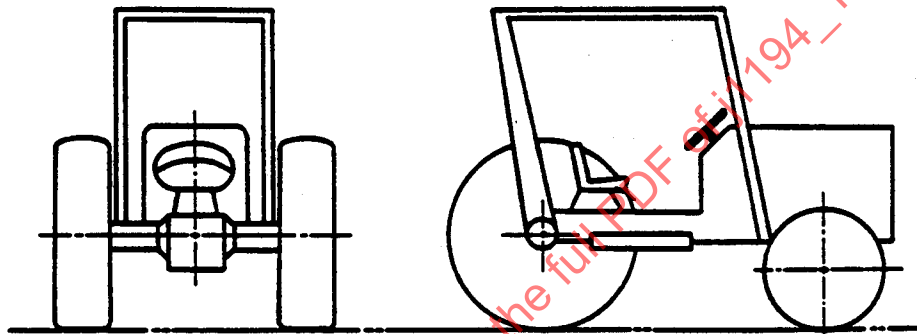


FIGURE 2—TRACTOR WITH TYPICAL FOUR-POST ROPS

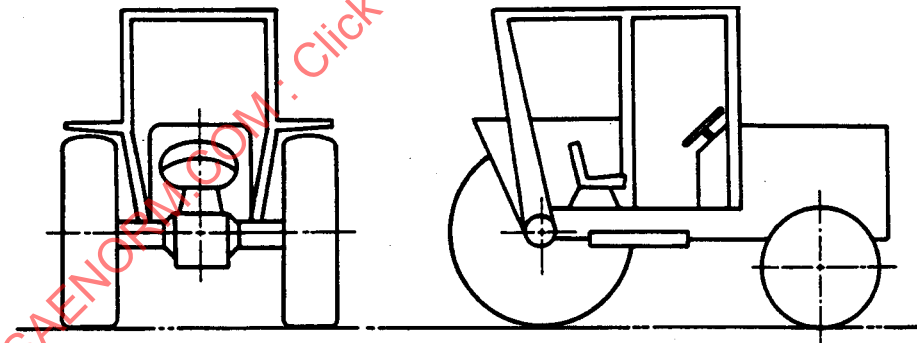


FIGURE 3—TRACTOR WITH TYPICAL PROTECTIVE ENCLOSURE

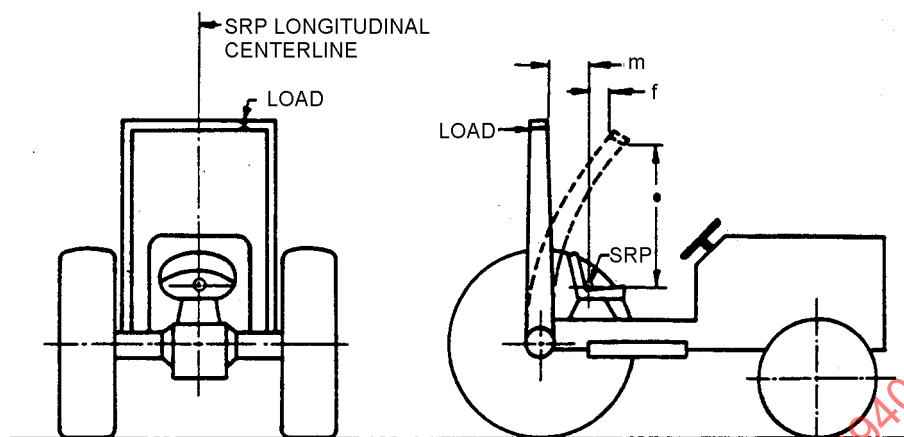


FIGURE 4—TYPICAL REAR LOAD APPLICATION

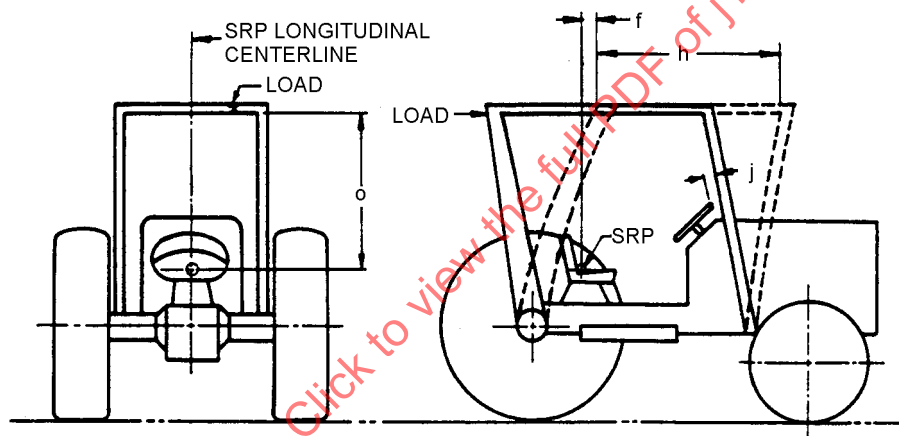


FIGURE 5—TYPICAL REAR LOAD APPLICATION

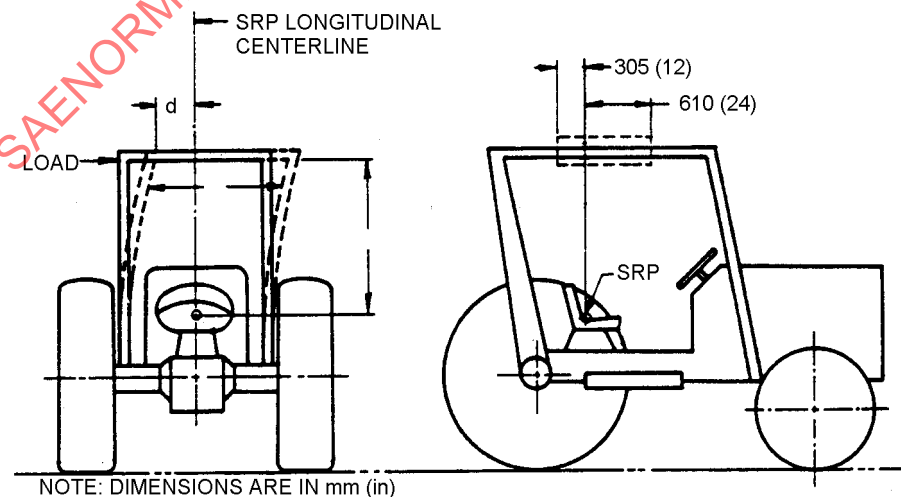


FIGURE 6—TYPICAL SIDE LOAD APPLICATION

4. General Requirements

- 4.1** Batteries, fuel tanks, oil reservoirs, and coolant systems shall be constructed and located or sealed to reduce the possibility of spillage which might be injurious to the operator in the event of upset.
- 4.2** All sharp edges and corners at the operator's station shall be appropriately treated to minimize operator injury in the event of upset.
- 4.3** Glazing shall conform to SAE J674.
- 4.4** Two or more operator exits shall be provided and positioned to reduce the possibility of all exits being blocked by the same accident.
- 4.5** Rear input energy tests (static, dynamic, or field upset) need not be performed on ROPS applied to tractors having four driven wheels and where the static vertical force reaction at the front wheels is greater than the static vertical force reaction at the rear wheels, since this type of tractor is not prone to rearward upset.
- 4.6** The tractor mass used shall be that of the heaviest tractor model on which the ROPS is to be used.
- 4.7** New ROPS and mounting connections of the same design shall be used for conducting the tests as described in the static (6.1), the dynamic (6.2), or the field upset procedure (6.4).
- 4.8** In case of an offset seat, the ROPS loading shall be on the side with the least space between the centerline of the seat and the protective structure.
- 4.9 Accuracy of Measurement**—(See Table 1.)

TABLE 1—ACCURACY OF MEASUREMENT

Measurement	Accuracy
Deflections of enclosure	±5% of deflection measured
Tractor mass	±5% of mass measured
Force applied to frame	±5% of force measured
Dimensions of critical zone	±12.7 mm (0.5 in)

- 4.10** Where movable or normally removable portions of the ROPS add to structural strength, they shall be placed in configurations that contribute least to the structural strength during the test.
- 4.11** If an overhead weather shield is available as an optional attachment to the protective structure, it may be in place during tests, provided it does not contribute to the strength of the protective structure.
- 4.12** If an overhead falling object protective cover is available as an optional attachment to the protective structure, it may be in place during tests provided it does not contribute to the strength of the protective structure.
- 4.13** No repairs or adjustments shall be made during the tests.
- 4.14** The protective structure shall meet the performance requirements established in Section 7.

5. Seat and Seat Belt Requirements

- 5.1** ROPS equipped tractors shall be fitted with seat belt assemblies (Type 1) conforming to the following, SAE J114, J117, J140, J141, J339, and J800 except as noted hereafter.

5.2 Where a suspended seat is used, the seat belt shall be fastened to the movable portion of the seat to accommodate the ride motion of the operator.

5.3 The seat belt anchorage shall be capable of withstanding a static tensile force of 4448 N (1000 lbf) at 45 degrees to the horizontal equally divided between the anchorages. The seat mounting shall be capable of withstanding this force plus a force equal to four times the force of gravity on the mass of all applicable seat components applied 45 degrees to the horizontal in a forward and upward direction. In addition, the seat mounting shall be capable of withstanding 2224 N (500 lbf) belt force plus two times the force of gravity on the mass of all applicable seat components both applied at 45 degrees to the horizontal in an upward and rearward direction. Floor and seat deformation is acceptable provided there is no structural failure or release of the seat adjuster mechanism or other locking device. The seat adjuster or locking device need not be operable after application of the test load.

6. Test Procedures

6.1 Static Test—(optional to 6.2).

6.1.1 TEST CONDITIONS

6.1.1.1 The ROPS mounting base shall be the tractor chassis or the equivalent for which the ROPS is designed to assure the integrity of the entire system.

6.1.1.2 The ROPS shall be instrumented with the necessary equipment to obtain the required load deflection data at the location and direction specified in Figures 4, 5, and 6. The measuring devices shall be located to record the force and deflection at the point of and along the line of loading. Load and deflection points shall be plotted in increments of deflection no greater than 12.7 mm (0.5 in). The rate of application of deflection (load) shall be such that it can be considered static.

6.1.2 DEFINITION OF TERMS

M = tractor mass as defined in 3.2 and 4.6:

Units: M in kg

M' in lb

E_{is} = energy input to be absorbed during side loading:

$E_{is} = 980 + 1.2 M$ units: J and kg

$E_{is'} = 8676 + 4.8 M'$ units: in-lbf and lb

E_{ir} = energy input to be absorbed during rear loading:

$E_{ir} = 1.4 M$ units: J and kg

$E_{ir'} = 5.64 M'$ units: in-lbf and lb

F = static load:

Units: F in N

F' in lbf

D = deflection under F:

Units: D in mm

D' in inches

EF-D = static force deflection curve

E_u = strain energy absorbed by the structure

E_u = area under F-D Curve:

Units: E_u in j

E_u in inches/lbf

6.1.3 STATIC TEST PROCEDURES

6.1.3.1 Apply the rear load per Figures 4 or 5 and record F and D simultaneously. Rear load application shall be uniformly distributed along a projected dimension no greater than 686 mm (27 in) and an area no greater than 0.1032 m^2 (160 in^2) normal to the direction of load application. The load shall be applied to the upper extremity of the ROPS at the point which is midway between the center of the ROPS and the inside of the ROPS upright. If no structural crossmember exists at the rear of the ROPS, a substitute test beam which does not add strength to the ROPS may be utilized to complete this test procedure. (See 6.4.1.1 if field upset is omitted.) Stop the test when:

- The strain energy absorbed by the structure is equal to or greater than the required input energy E_r (6.1.2) or
- Deflection of the structure exceeds the allowable deflection (7.1.1).

6.1.3.2 Using data obtained in 6.1.3.1, construct the F-D curve as shown typically in Figure 7 and calculate E_u .

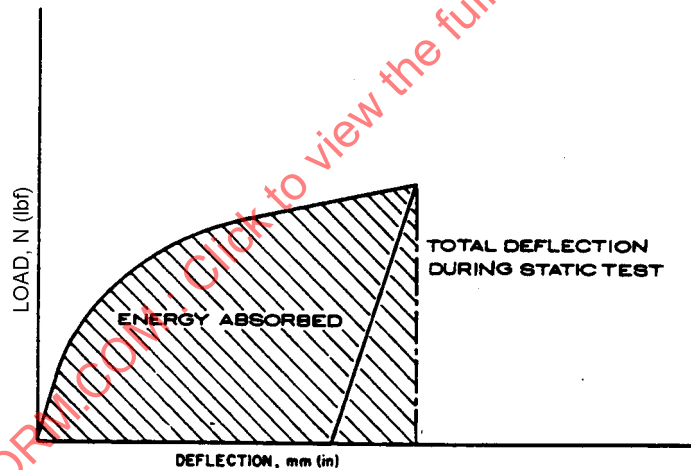


FIGURE 7—FORCE DEFLECTION (F-D) CURVE

6.1.3.3 Apply the side load as shown in Figure 6 and record F and D simultaneously. Static side load application shall be uniformly distributed along a projected dimension no greater than 686 mm (27 in) and an area no greater than 0.1032 m^2 (160 in^2) normal to the direction of load application. Side load application shall be at a 90 degree angle to the centerline of vehicle. The center of side load application shall be located between a distance 610 mm (24 in) forward, and a distance 305 mm (12 in) rearward of the seat reference point to best utilize the structural strength (see Figure 6). If the ROPS is a one or two post design, the side load shall be applied in line with the upper crossmember. The side load shall be applied to the longitudinal side farthest from the point of rear load application. (See 6.4.1.1 if field upset is omitted.) Stop the test when:

- The strain energy absorbed by the structure is equal to or greater than the required input energy E_{is} (6.1.2) or
- Deflection of the structure exceeds the allowable deflection (7.1.1).

6.1.3.4 Using data obtained in 6.1.3.3 construct the F-D curve as shown typically in Figure 7 and calculate E_u .

6.2 Dynamic Test—(optional to 6.1).

6.2.1 TEST CONDITIONS

6.2.1.1 The tractor shall be ballasted to achieve the mass as specified in Section 3 so that the static vertical force reaction at the front wheels shall be at least 33% of the static vertical force reaction at the rear wheels. The wheel tread setting, where adjustable, shall be at the position nearest to halfway between the minimum and maximum settings obtainable on the tractor. Where only two settings are obtainable, the minimum setting shall be used provided the tires do not interfere with structure deflection. The tires shall have no liquid ballast and shall be inflated to the maximum operating pressure recommended by the manufacturer.

6.2.1.2 The dynamic loading shall be produced by use of a 2000 kg (4410 lb) mass acting as a pendulum. The impact face of the mass shall be $686 \pm 25 \times 686 \pm 25$ mm ($27 \pm 1 \times 27 \pm 1$ in) and shall be constructed so that its center of gravity is within 25.4 mm (1 in) of its geometric center. The mass shall be suspended from a pivot point 5.5 to 6.7 m (18 to 22 ft) above the point of impact on the ROPS and shall be conveniently and safely adjustable for height (see Figure 8).

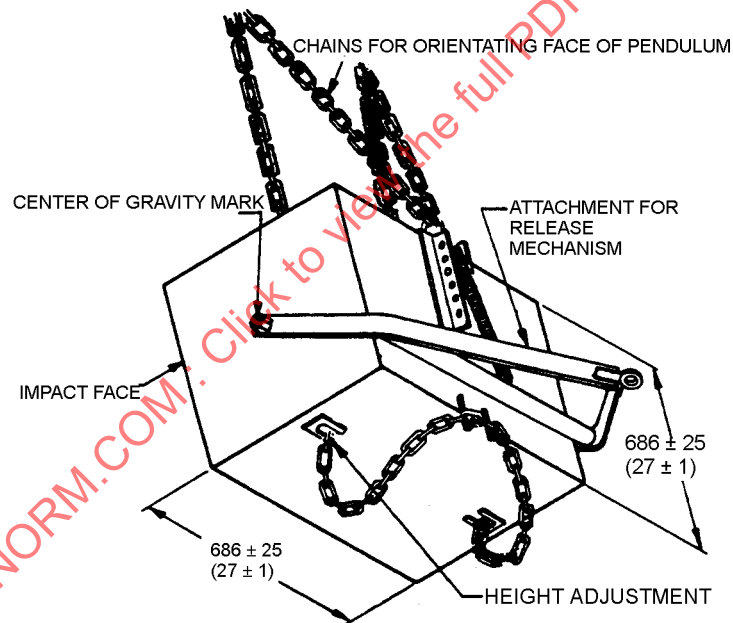


FIGURE 8—PENDULUM

- 6.2.1.3 For each phase of testing, the tractor shall be restrained from moving when the dynamic load is applied. The restraining members shall have strength no less than, and elasticity no greater than that of a 12.7 mm (0.50 in) diameter steel cable. Points of attaching restraining members shall be located an appropriate distance behind the rear axle and in front of the front axle to provide 15 to 30 degree angle between a restraining cable and the horizontal. For the impact from the rear, the restraining cables shall be located in the plane in which the center of gravity of the pendulum will swing or, alternatively, two sets of symmetrically located cables may be used at convenient lateral locations on the tractor. For the impact from the side, restraining cables shall be used as shown in Figures 9 and 10.

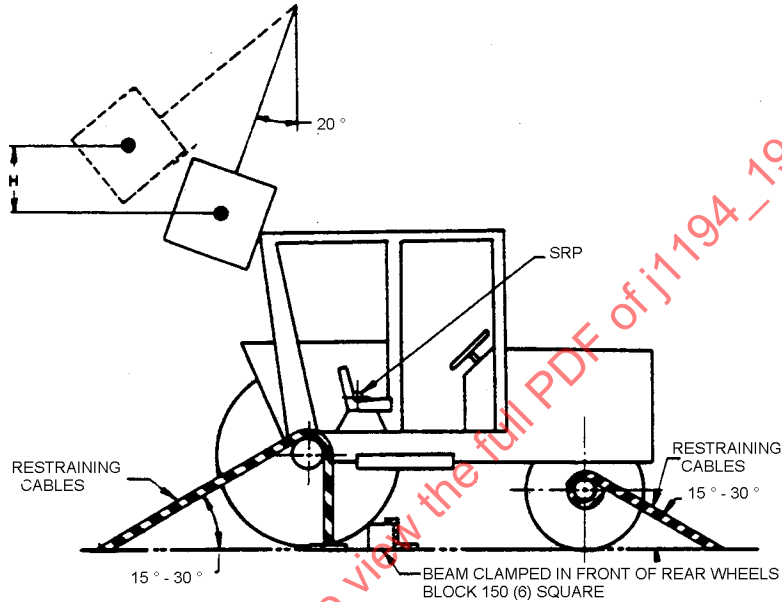


FIGURE 9—TYPICAL REAR IMPACT APPLICATION

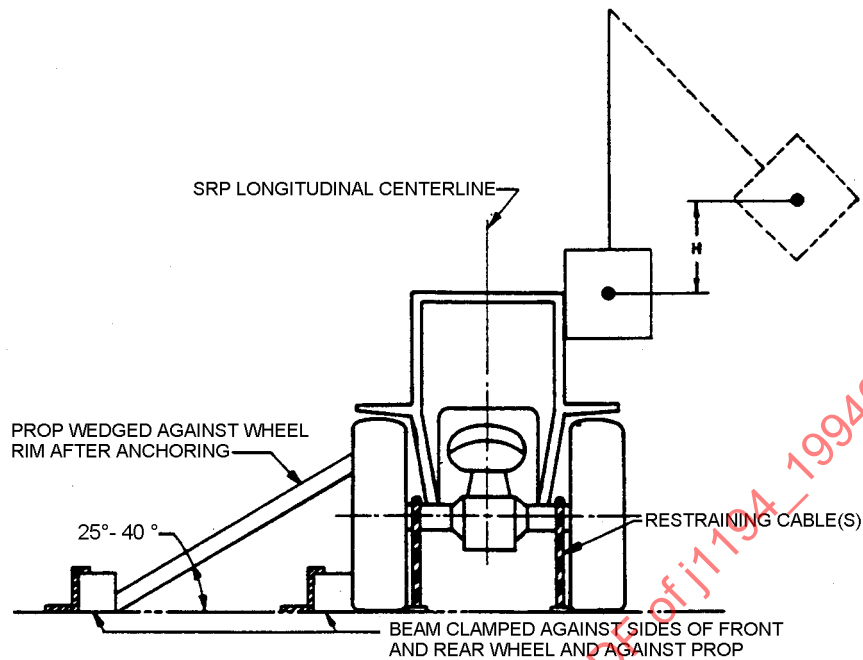


FIGURE 10—TYPICAL SIDE IMPACT APPLICATION

- 6.2.1.4 The restraining cable(s) shall be tightened to provide tire deflection of 6 to 8% of nominal tire section width. After the tractor is properly restrained, a beam no smaller than 150 × 150 mm (6 × 6 in) in cross section shall be driven tightly against the appropriate wheels and clamped. For the test to the side, an additional beam of sufficient strength to prevent rim displacement shall be placed as a prop against the wheel rim nearest the operator's station on the side opposite the pendulum impact and shall be secured to the base so it is held tightly against the wheel rim during impact. The length of this beam shall be chosen so that it is at an angle of 25 to 40 degrees to the horizontal when it is positioned against the wheel rim (Figures 9 and 10).
- 6.2.1.5 Means shall be provided for indicating the maximum instantaneous deflection relative to the SRP and parallel to the vertical plane of the pendulum swing. A simple friction device is illustrated in Figure 11.

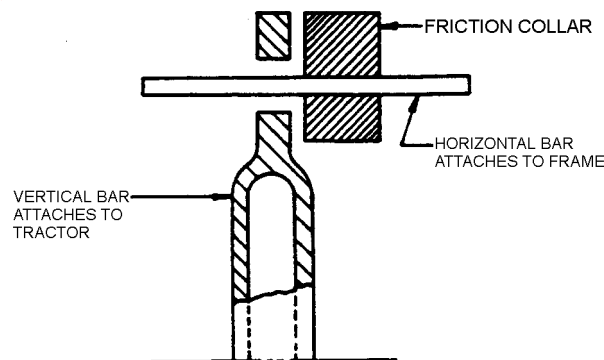


FIGURE 11—TYPICAL METHOD OF MEASURING DEFLECTION

6.2.1.6 If any cables, props, or blocking shift or break during the testing, the test shall be repeated.

6.2.2 DEFINITION OF TERMS

M = tractor mass as defined in Section 3 and 4.6:

Units: M in kg
M' in lb

H = vertical height of the pendulum mass:

Units: H in mm
H' in inches

The pendulum mass shall be 2000 kg (4410 lb).

The pendulum mass shall be pulled back so that the height of its center of gravity above the point of impact is as follows:

$H = 125 + 0.107M$ Units: mm and kg
 $H' = 4.92 + 0.0019M'$ Units: in and lb

6.2.3 DYNAMIC TEST PROCEDURES

6.2.3.1 The ROPS shall be evaluated by imposing dynamic loading from the rear, followed by a load to the side on the same ROPS. The pendulum swinging from the height determined by 6.2.2 imposes the dynamic load. The position of the pendulum shall be so selected that the initial point of impact on the ROPS shall be in line with the arc of travel of the center of gravity of the pendulum. A quick release mechanism should be used but shall not influence the attitude of the pendulum.

6.2.3.2 *Impact at Rear*—The tractor shall be properly restrained per 6.2.1.3 and 6.2.1.4. The tractor shall be positioned so that the supporting chains of the pendulum are at an angle of 20 degrees to the vertical when striking the structure as shown in Figure 9. If the angle of the cab or frame member at the point of contact is greater than 20 degrees forward of the vertical, the angle of the face of the pendulum shall be further adjusted by any convenient means so that the striking face of the pendulum and the cab or frame member are parallel. The impact shall be applied to the upper extremity of the ROPS at the point which is midway between the centerline of the ROPS and the inside of the ROPS upright. If no structural crossmember exists at the rear of the ROPS, a substitute test beam which does not add to the strength of the structure may be utilized to complete the test procedure.

6.2.3.3 *Impact at Side*—The tractor shall be properly restrained as per 6.2.1.3 and 6.2.1.4. The tractor shall be positioned so that the supporting chains of the pendulum are vertical when striking the structure as shown in Figure 10. If the structural member at the point of impact is not vertical, the angle of the face of the pendulum shall be adjusted by any convenient means so that the striking face of the pendulum and the cab or frame member are parallel.

The point of impact shall be at the upper extremity of the ROPS at a 90 degree angle to the centerline of the tractor and located between a distance 610 mm (24 in) forward, and a distance 305 mm (12 in) rearward of the seat reference point to best utilize the structural strength (see Figures 6 and 10). If the ROPS is a one or two post design, the side impact shall be applied in line with the upper crossmember. The side impact shall be applied to the longitudinal side farthest from the point of rear impact.

6.3 Crush Test Procedure

- 6.3.1 After the ROPS has been subjected to either static or dynamic loads, the same ROPS shall be subjected to a static crush test.
- 6.3.2 The test load shall be 1.5 times the gravity force of the tractor mass as defined and explained in Section 3. The manner of distributing this load on the ROPS shall be such to best utilize those structural members in the fore and aft plane which will support the tractor in an upset position. The resultant of the initial crushing force or load shall be in the vertical direction and shall be in a vertical plane passing through the SRP and parallel to the longitudinal axis of the tractor (Figure 12). The tractor chassis shall be rigidly supported during this test.

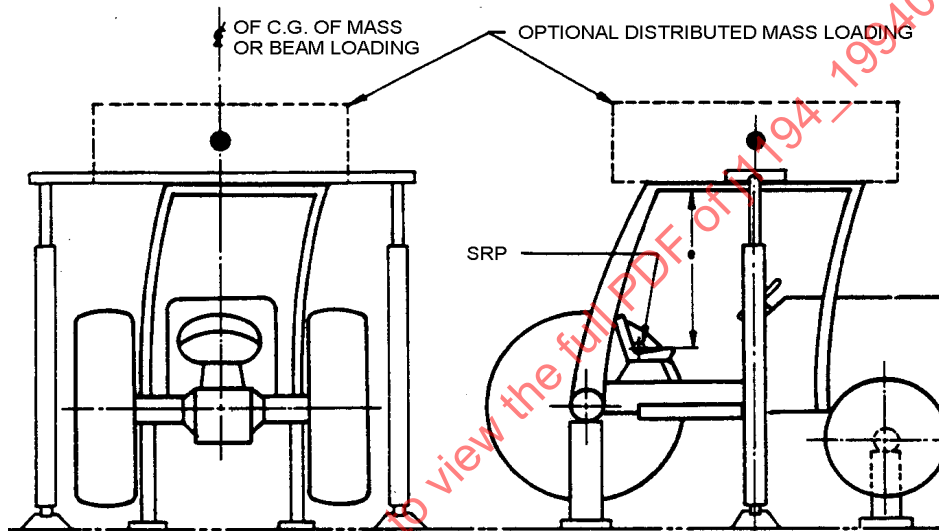


FIGURE 12—TYPICAL METHOD OF LOAD APPLICATION FOR CRUSH TEST

6.4 Field Upset Test

6.4.1 TEST CONDITIONS

- 6.4.1.1 The field upset test may be omitted if the ROPS laboratory test (static or dynamic) results indicate compliance at an energy application of 115% or more of the requirements defined in 6.1.2 or 6.2.2 and the ROPS meets the temperature-material requirements (see 7.1.2).
- 6.4.1.2 The tractor shall be ballasted to achieve the mass as specified in Section 3 so that the static vertical force reaction at the front wheels shall be at least 33% of the static vertical force reaction at the rear wheels. The wheel tread setting, where adjustable, shall be at the position nearest to halfway between the minimum and maximum settings of the shortest axles obtainable on the tractor. Where only two settings are obtainable, the minimum setting shall be used provided the tires do not interfere with structure deflection. The tires may have liquid ballast and shall be inflated to the maximum operating pressure recommended by the manufacturer.
- 6.4.1.3 The tests shall be conducted on a firm soil bank as shown in Figures 13 and 14. The soil in the impact area shall have an average cone index in the 0 to 152 mm (0 to 6 in) layer not less than 150. (Cone index is defined in ASAE R313.) The path of tractor travel shall be 12 degrees $\pm$ 2 degrees to the top edge of the bank. A 457 mm (18 in) high ramp as described and located in Figure 14 shall be used to assist in upsetting the tractor to its side.