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Thermoplastics pipes — Determination of ring stiffness

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Foreword

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International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft international Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 9969 was prepared by Technical Committee ISO/TC 138, Plastics pipes, fittings and valves for the transport of fluids, Subcommittee SC 5, General properties of pipes, fittings and valves of plastic materials and their accessories — Test methods and basic specifications.

This second edition cancels and replaces the first edition (ISO 9969:1994), which has been technically revised.

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Thermoplastics pipes — Determination of ring stiffness

1 Scope

This International Standard specifies a test method for determining the ring stiffness of thermoplastics pipes having a circular cross section.

2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the datest edition of the referenced document (including any amendments) applies.

ISO 3126, Plastics piping systems — Plastics components — Determination of dimensions

3 Symbols

For the purposes of this document, the following symbols apply.

		Units
d_{n}	nominal diameter of pipe	mm
d_{i}	inside diameter of pipe	Cmm
e_{c}	construction height	mm
F	force (of loading)	kN
L	length of the test piece	mm
p	pitch of ribs or windings	mm
S	ring stiffness	kN/m ²
У	wertical deflection	mm
S	ring stiffness	kN/m ²

4 Principle

The ring stiffness is determined by measuring the force and the deflection while deflecting the pipe at a constant deflection speed.

A cut length of pipe supported horizontally is compressed vertically between two parallel flat plates moved at a constant speed that is dependent upon the diameter of the pipe.

A plot of force versus deflection is generated. The ring stiffness is calculated as a function of the force necessary to produce a 3 % diametric deflection of the pipe.

NOTE It is assumed that the test temperature is set by the referring standard, if appropriate (see 8.1).

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5 Apparatus

5.1 Compressive testing machine, capable of a constant rate of crosshead movement, via a pair of parallel plates (5.2), as appropriate to the nominal diameter of the pipe in conformance with Table 1, with sufficient force and travel to produce the specified diametric deflection (see Clause 8).

Nominal diameter, $d_{\rm n}$, of pipe mm	Deflection speed mm/min	
<i>d</i> _n ≤ 100	$2\pm0,1$	
$100 < d_{n} \leqslant 200$	$5\pm0,\!25$	
$200 < d_{n} \leqslant 400$	$10 \pm 0{,}5$	
$400 < d_{n} \leqslant 710$	20 ± 1	00
$d_{\sf n} > 710$	$0.03 imes d_{ extsf{i}} \pm 5$ % ^a	000
$d_{\rm i}$ shall be determined in accordance with 6.3.	. (.0

Table 1 — Deflection speeds

5.2 A pair of hard and rigid plates, through which the testing machine can apply the necessary force, F, to the test piece.

The plates shall have flat, smooth and clean surfaces for contact with the test piece.

The stiffness and hardness of each plate shall be sufficient to prevent bending or deformation to an extent that would affect the results.

The length of each plate shall be at least equal to the length of the test piece. The width of each plate shall not be less than the width of the contact surface with the test piece while under load plus 25 mm.

5.3 Dimensional measuring devices, capable of determining

- individual values for the length of a test piece (see 6.2.2 and 6.2.3) to within 1 mm,
- the inside diameter of a test piece to within 0,5 %, and
- the change of inside diameter of a test piece in the direction of loading with an accuracy of 0,1 mm or 1 % of the deflection, whichever is the greater.

An example of a device for measuring the inside diameter of corrugated pipe is shown in Figure 1.

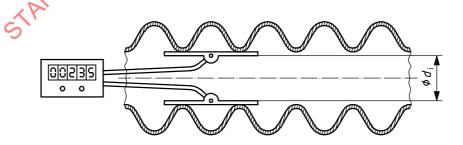


Figure 1 — Example of device for measuring inside diameter of corrugated pipe

5.4 Force measuring device, capable of determining to within 2 % the force necessary to produce a deflection of up to 4 % of the test piece.

6 Test pieces

6.1 Marking and number of test pieces

The pipe of which the ring stiffness is to be determined shall be marked on its outside with a line along one generatrix over its entire length. Three test pieces, a, b and c, respectively, shall be taken from this marked pipe such that the ends of the test pieces are perpendicular to the pipe axis and their lengths conform to 6.2.

6.2 Length of test pieces

6.2.1 The length of each test piece shall be determined by calculating the arithmetic average of three to six measurements of length equally spaced around the perimeter of the pipe, as given in Table 2. The length of each test piece shall conform to 6.2.2, 6.2.3, 6.2.4 or 6.2.5, as applicable.

Each of the three to six length measurements shall be determined to within 1 mm.

For each individual test piece, the smallest of the three to six measurements shall not be less than 0,9 times the largest length measurement.

Nominal diameter, $d_{\rm n}$, of pipe mm Number of length measurements $d_{\rm n} \leqslant 200 \qquad \qquad 3$ $200 < d_{\rm n} < 500 \qquad \qquad 4$ $d_{\rm n} \geqslant 500 \qquad \qquad 6$

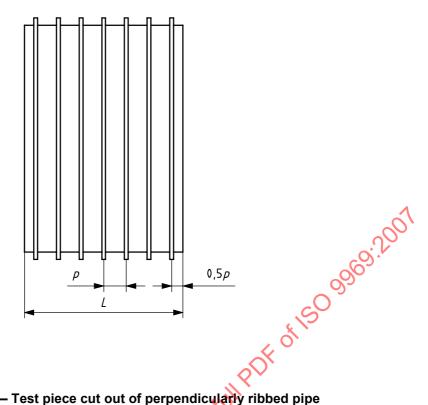
Table 2 — Number of length measurements

- **6.2.2** For pipes that have nominal diameters equal to or less than 1 500 mm, the average length of the test pieces shall be (300 ± 10) mm.
- **6.2.3** For pipes that have nominal diameters larger than 1 500 mm, the average length of the test pieces in millimetres shall be at least $0.2d_n$
- **6.2.4** Structured wall pipes with perpendicular ribs, corrugations or other regular structures shall be cut such that each test piece contains a whole number of ribs, corrugations or other structures. The cuts shall be made at the mid point between the ribs, corrugations or other structures.

The length of the test pieces shall be the minimum whole number of ribs, corrugations or other structures resulting in a length of 290 mm or greater or, for pipes greater than 1 500 mm, $0.2d_n$ or greater.

See Figure 2.

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Key

- test piece length
- pitch

Figure 2 — Test piece cut out of perpendicularly ribbed pipe

Structured wall pipes with helical ribs, corrugations or other regular structures shall be cut such that the length of the test pieces is equal to the inside diameter 20 mm but not less than 290 mm nor greater than 1 000 mm.

Inside diameter of test piece(s) 6.3

The inside diameters, d_{ia} , d_{ib} and d_{ic} , of the respective test pieces, a, b and c (see 6.1), shall be determined either as

- the arithmetic average of four measurements at 45° intervals of one cross section at mid-length, where a) each measurement shall be determined to within 0,5 %, or
- measured at mid-length cross-section by means of a π tape in accordance with ISO 3126.

The calculated or measured average inside diameter for each test piece, a, b and c, shall be recorded, as d_{ia} , d_{ib} and d_{ic} , respectively.

The average value, d_i , of these three calculated values shall be calculated using Equation (1):

$$d_{\rm i} = \frac{d_{\rm ia} + d_{\rm ib} + d_{\rm ic}}{3} \tag{1}$$

Age of test pieces

At the start of testing in accordance with Clause 8, the age of the test pieces shall be at least 24 h.

For type testing, and in case of dispute, the age of the test pieces shall be (21 ± 2) days.

7 Conditioning

The test pieces shall be conditioned in air at the test temperature (see 8.1) for at least 24 h immediately prior to testing in accordance with Clause 8.

8 Procedure

8.1 Unless otherwise specified in the referring standard, carry out the following procedure at (23 ± 2) °C or, in countries where 27 °C is used as standard laboratory temperature, at (27 ± 2) °C.

In case of dispute, (23 \pm 2) °C shall be used.

NOTE It is probable that the test temperature has an influence on the ring stiffness.

8.2 If it can be determined in which position the test piece has the lowest ring stiffness, place the first piece, a, in this position in the loading device.

Otherwise, place the first test piece in such a way that the marking line is in contact with the upper parallel plate.

In the loading device, rotate the two other test pieces, b and c, respectively 120° and 240° in relation to the position of the first test piece when placing them in their loading devices.

8.3 For each test piece, attach the deflection gauge and check the angular position of the test piece in relation to the upper plate.

Position the test piece with its longitudinal axis parallel to the plates and with its middle point vertically under the centre-line of the load cell.

NOTE In order to obtain the correct reading from the load cell, it is necessary to position the test piece so the expected resulting force is approximately in line with the axis of the load cell.

8.4 Lower the loading plate until it touches the upper part of the test piece.

Apply one of the following pre-load forces, F_0 , as applicable, rounded up to the nearest newton if calculated from Equation (2), taking into account as applicable the mass of the loading plate:

- a) for pipes with d_i less than or equal to 100 mm, F_0 shall be 7,5 N;
- b) for pipes with d_i larger than 100 mm, F_0 shall be calculated using Equation (2) in newtons and the result rounded up where necessary to the next higher newton:

$$F_0 = 250 \times 10^{-6} d_{\rm n} \times L \tag{2}$$

where

down is the nominal diameter of the pipe, in millimetres;

L is the actual length of the test piece, in millimetres.

The actually applied pre-load force shall be between 95 % and 105 % of the calculated force when measured with the accuracy possible with the load cell used for the test.

Then adjust the deflection gauge and load cell to zero.

In case of dispute, the zero adjustment method shall be used, see 8.6.

8.5 Compress the test piece at a constant speed in accordance with Table 1, while continuously recording force and deflection measurements in conformance with 8.6, until reaching a deflection of at least $0.03d_i$.

NOTE When determination of ring flexibility is required, the deflection can be continued until the deflection required for ring flexibility has been reached.

Typically, the force and deflection measurements are generated continuously by measuring the displacement of one of the flat plates, but if during the test the pipe wall construction height, e_c (see Figure 3), changes by more than 5 %, generate the force/deflection plot by measuring the change of the inside diameter of the test piece.

In case of dispute, the change of the inside diameter shall be used as a reference.

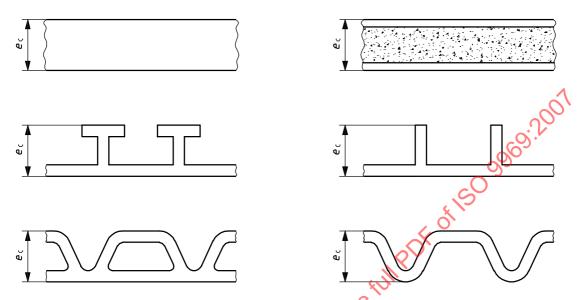
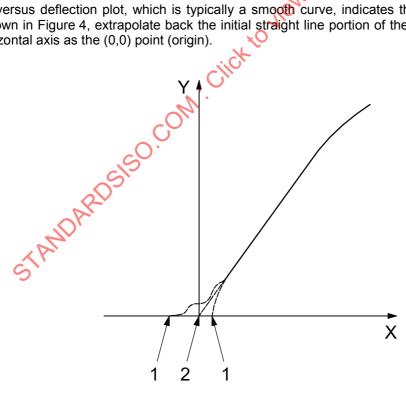


Figure 3 — Examples of the pipe wall construction height, e_c

If the force versus deflection plot, which is typically a smooth curve, indicates that the zero point may be in error, as shown in Figure 4, extrapolate back the initial straight line portion of the curve and use the intersect with the horizontal axis as the (0,0) point (origin).



Key

- deflection, y Χ
- force, F
- apparent zero
- corrected zero

Figure 4 — Method of correcting origin

9 Calculation of ring stiffness

Calculate the ring stiffness, $S_{\rm a}$, $S_{\rm b}$ and $S_{\rm c}$, of each of the three test pieces (a, b and c, respectively), in kilonewtons per square metre, using the following equations:

$$S_{a} = \left(0,0186 + 0,025 \frac{y_{a}}{d_{i}}\right) \frac{F_{a}}{L_{a}y_{a}} \times 10^{6}$$
(3)

$$S_{b} = \left(0.0186 + 0.025 \frac{y_{b}}{d_{i}}\right) \frac{F_{b}}{L_{b}y_{b}} \times 10^{6}$$
(4)

$$S_{c} = \left(0,0186 + 0,025 \frac{y_{c}}{d_{i}}\right) \frac{F_{c}}{L_{c}y_{c}} \times 10^{6}$$
(5)

where

F is the force, in kilonewtons, that corresponds to a 3,0 % pipe deflection;

L is the length of the test piece, in millimetres;

y is the deflection, in millimetres, that corresponds to a 3,0 % deflection, i.e.

$$\frac{y}{d_i} = 0.03$$

Calculate the ring stiffness of the pipe, S, in kilonewtons per square metre, as the average of these three values, using Equation (6):

$$S = \frac{S_a + S_b + S_c}{3} \tag{6}$$

10 Test report

The test report shall include the following information:

- a) reference to this International Standard (i.e. ISO 9969:2007) and to the referring standard, if any;
- b) the identification of the thermoplastics pipe, including
 - 1) manufacturer,
 - 2) type of pipe (including material),
 - 3) dimensions,
 - 4) nominal stiffness and/or pressure class,
 - 5) production date,
 - 6) lengths of test pieces, and
 - 7) mass per metre length of the pipe;