

# INTERNATIONAL STANDARD

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Edition 1:1995 consolidated with amendment 1:2000

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BASIC EMC PUBLICATION

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## Electromagnetic compatibility (EMC) –

### Part 4-5: Testing and measurement techniques – Surge immunity test

*This **English-language** version is derived from the original **bilingual** publication by leaving out all French-language pages. Missing page numbers correspond to the French-language pages.*



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### **Part 4-5: Testing and measurement techniques – Surge immunity test**

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International Electrotechnical Commission  
Международная Электротехническая Комиссия

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## INTERNATIONAL ELECTROTECHNICAL COMMISSION

**ELECTROMAGNETIC COMPATIBILITY (EMC) –****Part 4-5: Testing and measurement techniques –  
Surge immunity test****FOREWORD**

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International Standard IEC 61000-4-5 has been prepared by subcommittee 65A: System aspects, of IEC technical committee 65: Industrial-process measurement and control.

It forms section 5 of part 4 of IEC 61000. It has the status of a basic EMC publication in accordance with IEC Guide 107.

This consolidated version of IEC 61000-4-5 is based on the first edition (1995), [documents 65A(CO)41+77B(CO)25 and 65A/168/RVD] and its amendment 1 (2000) [documents 77B/291+293/FDIS and 77B/298+300/RVD].

It bears the edition number 1.1.

A vertical line in the margin shows where the base publication has been modified by the corrigendum and amendment 1.

Annex A forms an integral part of this standard.

Annexes B and C are for information only.

The committee has decided that the contents of the base publication and its amendment 1 will remain unchanged until 2003. At this date, the publication will be

- reconfirmed;
- withdrawn;
- replaced by a revised edition, or
- amended.

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## INTRODUCTION

This standard is part of the IEC 61000 series, according to the following structure:

**Part 1: General**

General considerations (introduction, fundamental principles)

Definitions, terminology

**Part 2: Environment**

Description of the environment

Classification of the environment

Compatibility levels

**Part 3: Limits**

Emission limits

Immunity limits (in so far as they do not fall under the responsibility of the product committees)

**Part 4: Testing and measurement techniques**

Measurement techniques

Testing techniques

**Part 5: Installation and mitigation guidelines**

Installation guidelines

Mitigation methods and devices

**Part 9: Miscellaneous**

Each part is further subdivided into sections which are to be published either as international standards or as technical reports.

This section is an international standard which gives immunity requirements and test procedures related to surge voltages and surge currents.



## **ELECTROMAGNETIC COMPATIBILITY (EMC) –**

### **Part 4-5: Testing and measurement techniques – Surge immunity test**

#### **1 Scope and object**

This section of IEC 61000-4 relates to the immunity requirements, test methods, and range of recommended test levels for equipment to unidirectional surges caused by overvoltages from switching and lightning transients. Several test levels are defined which relate to different environment and installation conditions. These requirements are developed for and are applicable to electrical and electronic equipment.

The object of this section is to establish a common reference for evaluating the performance of equipment when subjected to high-energy disturbances on the power and interconnection lines.

This standard defines:

- range of test levels;
- test equipment;
- test set-up;
- test procedure.

The task of the described laboratory test is to find the reaction of the EUT under specified operational conditions caused by surge voltages from switching and lightning effects at certain threat levels.

It is not intended to test the capability of the insulation to withstand high-voltage stress. Direct lightning is not considered in this standard.

This standard does not intend to specify the tests to be applied to particular apparatus or systems. Its main aim is to give a general basic reference to all concerned product committees of the IEC. The product committees (or users and manufacturers of equipment) remain responsible for the appropriate choice of the tests and the severity level to be applied to their equipment.

#### **2 Normative references**

The following normative documents contain provisions which, through reference in this text, constitute provisions of this section of IEC 61000-4. At the time of publication, the editions indicated were valid. All normative documents are subject to revision, and parties to agreements based on this section of IEC 61000-4 are encouraged to investigate the possibility of applying the most recent editions of the normative documents indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

IEC 60050(161):1990, *International Electrotechnical Vocabulary (IEV) – Chapter 161: Electromagnetic compatibility*

IEC 60060-1:1989, *High-voltage test techniques – Part 1: General definitions and test requirements*

IEC 60469-1:1987, *Pulse techniques and apparatus – Part 1: Pulse terms and definitions*

### 3 General

#### 3.1 Switching transients

System switching transients can be separated into transients associated with:

- a) major power system switching disturbances, such as capacitor bank switching;
- b) minor switching activity near the instrumentation or load changes in the power distribution system;
- c) resonating circuits associated with switching devices, such as thyristors;
- d) various system faults, such as short circuits and arcing faults to the earthing system of the installation.

#### 3.2 Lightning transients

The major mechanisms by which lightning produces surge voltages are the following:

- a) a direct lightning stroke to an external circuit (outdoor) injecting high currents producing voltages by either flowing through earth resistance or flowing through the impedance of the external circuit;
- b) an indirect lightning stroke (i.e. a stroke between or within clouds or to nearby objects which produces electromagnetic fields) that induces voltages/currents on the conductors outside and/or inside a building;
- c) lightning earth current flow resulting from nearby direct-to-earth discharges coupling into the common earth paths of the earthing system of the installation.

The rapid change of voltage and flow of current which may occur when a protector is excited may couple into internal circuits.

#### 3.3 Simulation of the transients

- a) The characteristics of the test generator are such that it simulates the above-mentioned phenomena as closely as possible;
- b) if the source of interference is in the same circuit, e.g. in the power supply network (direct coupling), the generator may simulate a low impedance source at the ports of the equipment under test;
- c) if the source of interference is not in the same circuit (indirect coupling) as the ports of the victim-equipment, then the generator may simulate a higher impedance source.

## 4 Definitions

For the purposes of this section of IEC 61000-4, the following definitions together with those in IEC 60050(161) apply, unless otherwise stated.

### 4.1

#### **balanced lines**

a pair of symmetrically driven conductors with a conversion loss from differential to common mode of less than 20 dB

### 4.2

#### **coupling network**

electrical circuit for the purpose of transferring energy from one circuit to another

### 4.3

#### **decoupling network**

electrical circuit for the purpose of preventing surges applied to the EUT from affecting other devices, equipment or systems which are not under test

### 4.4

#### **duration**

the absolute value of the interval during which a specified waveform or feature exists or continues. [IEC 60469-1]

### 4.5

#### **EUT**

equipment under test

### 4.6 front time

#### **surge voltage**

the front time  $T_1$  of a surge voltage is a virtual parameter defined as 1,67 times the interval  $T$  between the instants when the impulse is 30 % and 90 % of the peak value (see figure 2)

#### **current surge**

the front time  $T_1$  of a surge current is a virtual parameter defined as 1,25 times the interval  $T$ , between the instants when the impulse is 10 % and 90 % of the peak value (see figure 3). [IEC 60060-1 modified]

### 4.7

#### **immunity**

the ability of a device, equipment or system to perform without degradation in the presence of an electromagnetic disturbance. [IEV 161-01-20]

### 4.8

#### **electrical installation**

an assembly of associated electrical equipment to fulfil a specific purpose or purposes and having coordinated characteristics. [IEV 826-01-01]

#### 4.9

**interconnection lines** consist of:

- I/O lines (input/output lines);
- communication lines;
- balanced lines.

#### 4.10

##### **primary protection**

the means by which the majority of stressful energy is prevented from propagating beyond the designated interface

#### 4.11

##### **rise time**

the interval of time between the instants at which the instantaneous value of a pulse first reaches a specified lower value and then a specified upper value

NOTE Unless otherwise specified, the lower and upper values are fixed at 10 % and 90 % of the pulse magnitude. [IEV 161-02-05]

#### 4.12

##### **secondary protection**

the means by which the let-through energy from primary protection is suppressed. It may be a special device or an inherent characteristic of the EUT

#### 4.13

##### **surge**

a transient wave of electrical current, voltage, or power propagating along a line or a circuit and characterized by a rapid increase followed by a slower decrease. [IEV 161-08-11 modified]

#### 4.14

##### **system**

set of interdependent elements constituted to achieve a given objective by performing a specified function

NOTE The system is considered to be separated from the environment and other external systems by an imaginary surface which cuts the links between them and the considered system. Through these links, the system is affected by the environment, is acted upon by the external systems, or acts itself on the environment or the external systems. [IEV 351-01-01]

#### 4.15

##### **time to half-value $T_2$**

the time to half-value  $T_2$  of a surge is a virtual parameter defined as the time interval between the virtual origin  $O_1$  and the instant when the voltage current has decreased to half the peak value. [IEC 60060-1 modified]

#### 4.16

##### **transient**

pertaining to or designating a phenomenon or a quantity which varies between two consecutive steady states during a time interval short compared to the time-scale of interest. [IEV 161-02-01]

## 5 Test levels

The preferential range of test levels is given in table 1.

**Table 1 – Test levels**

Level	Open-circuit test voltage $\pm 10\%$ kV
1	0,5
2	1,0
3	2,0
4	4,0
x	Special
NOTE x is an open class. This level can be specified in the product specification..	

The test levels shall be selected according to the installation conditions; classes of installation are given in B.3 of annex B.

All voltages of the lower test levels shall be satisfied (see 8.2).

For selection of the test levels for the different interfaces, see annex A.

## 6 Test instrumentation

### 6.1 Combination wave (hybrid) generator (1,2/50 $\mu$ s - 8/20 $\mu$ s)

A simplified circuit diagram of the generator is given in figure 1. The values for the different components  $R_{S1}$ ,  $R_{S2}$ ,  $R_m$ ,  $L_r$  and  $C_c$  are selected so that the generator delivers a 1,2/50  $\mu$ s voltage surge (at open-circuit conditions) and a 8/20  $\mu$ s current surge into a short circuit, i.e. the generator has an effective output impedance of 2  $\Omega$ .

For convenience, an effective output impedance is defined for a surge generator by calculating the ratio of peak open-circuit output voltage and peak short-circuit current.

Such a generator with 1,2/50  $\mu$ s open-circuit voltage waveform 8/20  $\mu$ s short-circuit current waveform is referred to as a combination wave generator (CWG) or hybrid generator.

NOTE 1 The waveform of the voltage and current is a function of the EUT input impedance. This impedance may change during surges to equipment and due either to proper operation of the installed protection devices, or to flashover or component breakdown, if the protection devices are absent or inoperative. Therefore the 1,2/50  $\mu$ s voltage and the 8/20  $\mu$ s current waves have to be available from the same test generator output as instantaneously required by the load.

NOTE 2 The combination wave generator described in this standard is identical to the hybrid generator sometimes specified in some other standards.

### 6.1.1 Characteristics and performance of the combination wave generator

Open-circuit output voltage:

At least as low as	0,5 kV to at least as high as 4,0 kV
Waveform of the surge voltage	see figure 2 and table 2
Tolerance of the open circuit output voltage	±10 %

Short-circuit output current:

At least as low as	0,25 kA to at least as high as 2,0 kA
Waveform of the surge current	see figure 3 and table 2
Tolerance of the short-circuit output current	±10 %

Polarity positive/negative

Phase shifting in a range between 0° to 360° versus the a.c. line phase angle

Repetition rate at least 1 per min

A generator with floating output shall be used.

Additional resistors (10  $\Omega$  or 40  $\Omega$ ) shall be included to increase the required effective source impedances for the specified test conditions (see clause 7 and B.1 of annex B).

Under these circumstances, the open-circuit voltage waveform and the short-circuit current waveform in combination with the coupling/decoupling network are no longer 1,2/50  $\mu$ s and 8/20  $\mu$ s respectively (combination wave).

### 6.1.2 Verification of the characteristics of the generator

In order to compare the test results from different test generators, the test generator characteristic shall be verified. For this purpose, the following procedure is necessary to measure the most essential characteristics of the generator.

The test generator output shall be connected to a measuring system with a sufficient bandwidth and voltage capability to monitor the characteristics of the waveforms.

The characteristics of the generator shall be measured under open-circuit conditions (load greater or equal to 10 k $\Omega$ ) and under short-circuit conditions (load smaller or equal to 0,1  $\Omega$ ) at the same charge voltage.

NOTE Short-circuit current: 0,25 kA minimum with the open-circuit voltage set to 0,5 kV and 2,0 kA minimum with the open-circuit voltage set to 4,0 kV.

### 6.2 Test generator 10/700 $\mu$ s according to CCITT

The simplified circuit diagram of the generator is given in figure 4. The values for the different components  $R_c$ ,  $C_c$ ,  $R_s$ ,  $R_{m1}$ ,  $C_s$  and  $R_{m2}$  are defined so that the generator delivers a 10/700  $\mu$ s surge.

### 6.2.1 Characteristics and performances of the generator

Open-circuit output voltage:

At least as low as	0,5 kV to at least as high as 4,0 kV
Waveform of the surge voltage	see figure 5 (IEC 60060-1) and table 3
Tolerance of the open-circuit output voltage	±10 %

Short-circuit output current:

At least as low as	12,5 A to at least as high as 100 A
Waveform of the surge current	see table 3
Tolerance of the short-circuit output current	±10 %

Polarity positive/negative

Repetition rate at least 1 per min

A generator with floating output shall be used.

### 6.2.2 Verification of the characteristics of the generator

The verification conditions for the 10/700  $\mu$ s test generator are identical to 6.1.2 with the following note.

NOTE Short-circuit current: 12,5 A minimum with the open-circuit voltage set to 0,5 kV, and 100 A minimum with the open-circuit voltage set to 4,0 kV.

## 6.3 Coupling/decoupling networks

The coupling/decoupling networks shall not significantly influence the parameters of the generators e.g. open-circuit voltage, short-circuit current capability as in the specified tolerances.

*Exception:* Coupling via arrestor.

NOTE Lossy material for the inductances reduces ringing.

Each coupling/decoupling network shall satisfy the following requirements.

### 6.3.1 Coupling/decoupling networks for a.c./d.c. power supply circuits (only used with combination wave generator)

The front time and surge time to half value shall be verified for voltage under open-circuit conditions and for current under short-circuit conditions.

The test generator output or its coupling network shall be connected to a measuring system with a sufficient bandwidth and voltage capability to monitor the open-circuit voltage waveform.

The short-circuit current waveform can be measured with a current transformer through whose aperture passes a short-circuit link between the output terminals of the coupling network.

All waveform definitions, as well as all other performance parameters of the test generator, should be as specified in 6.1.1 at the output of the coupling/decoupling network as well as at the output of the generator itself.

NOTE When the generator impedance is increased from  $2\ \Omega$  to e.g.  $12\ \Omega$  or  $42\ \Omega$  according to the requirements of the test set-up, the duration of the test pulse at the output of the coupling network might be significantly changed.

### 6.3.1.1 Capacitive coupling for power supply circuits

Capacitive coupling enables the test voltage to be applied line to line or one line to earth while the power supply decoupling network is also connected. The circuit diagrams for single phase systems are shown in figures 6 and 7 and for three-phase systems are shown in figures 8 and 9.

Rated characteristics of the coupling/decoupling network:

*Coupling:*

coupling capacitors:  $C = 9\ \mu\text{F}$  or  $18\ \mu\text{F}$  (see test set-up)

*Decoupling:*

decoupling inductance for supply voltage:  $L = 1,5\ \text{mH}$

The residual surge voltage on unsurged lines shall not exceed 15 % of the maximum applicable test voltage when the EUT is disconnected.

The residual surge voltage on the power supply inputs of the decoupling network when the EUT and the power supply network are disconnected, shall not exceed 15 % of the applied test voltage or twice peak value of the power line voltage whichever is higher.

The above-mentioned characteristics for single-phase systems (line, neutral, protective earth) are also valid for three-phase systems (three-phase wires, neutral and protective earth).

### 6.3.1.2 Inductive coupling for power supply

Under consideration.

### 6.3.2 Coupling/decoupling networks for interconnection lines

The coupling method shall be selected as a function of the circuits and operational conditions. This has to be specified in the product specification.

Examples of coupling methods are the following:

- capacitive coupling;
- coupling via arrestors.

The different set-ups defined in the following subclauses to test a given port of the EUT may not give comparable results. The most suitable set-up has to be selected in the product specification/standard.

NOTE  $R_L$  in figures 10 to 12 represents the resistive part of the inductance  $L$  and the value is dependent on negligible attenuation of the transmission signal.



### 6.3.2.1 Capacitive coupling for interconnection lines

The capacitive coupling is the preferred method for unbalanced unshielded I/O circuits when there is no influence to the functional communication on that line. The application is in accordance with figure 10 for line-to-line coupling and for line-to-earth coupling.

Rated characteristics of the capacitive coupling/decoupling network:

Coupling capacitor  $C$ : 0,5  $\mu\text{F}$

Decoupling inductors  $L$  (not current compensated): 20 mH

NOTE Signal current capability has to be considered and is dependent on the circuits under test.

### 6.3.2.2 Coupling via arrestors

Coupling via arrestors is the preferred coupling method for unshielded balanced circuits (telecommunication), as shown in figure 12.

The method can also be used in cases where the capacitive coupling is not possible because of functional problems caused by attachment of capacitors to the EUT (see figure 11).

The coupling network also has the task to accommodate the distribution of the surge current in the case of induced voltages in multiconductor cables.

Therefore the resistances  $R_{m2}$  in the coupling network shall be, for  $n$  composite conductors,  $n \times 25 \Omega$  (for  $n$  equal to or greater than 2).

EXAMPLE:  $n = 4$ ,  $R_{m2} = 4 \times 25 \Omega$ . With the impedance of the generator the total value is approximately 40  $\Omega$ .  $R_{m2}$  shall not exceed 250  $\Omega$ .

The coupling via gas-filled arrestors can be improved by capacitors in parallel with the arrestors.

EXAMPLE:  $C \leq 0,1 \mu\text{F}$  for frequencies of the transmission signal on the line below 5 kHz. At higher frequencies no capacitors are used.

Rated characteristics of the coupling/decoupling network:

- coupling resistance  $R_{m2}$   $n \times 25 \Omega$  (for  $n$  equal to or greater than 2)
- arrestor (gas-filled) 90 V
- decoupling inductor  $L$  20 mH  
(ring core, current compensated)

NOTE 1 In some cases, arrestors with higher activation voltages are used for functional reasons.

NOTE 2 Other elements than arrestors may be used when the operational conditions are not unduly influenced.

### 6.3.3 Other coupling methods

Other coupling methods are under consideration.

## 7 Test set-up

### 7.1 Test equipment

The following equipment is part of the test set-up:

- equipment under test (EUT);
- auxiliary equipment (AE);
- cables (of specified type and length);
- coupling device (capacitive or arrestors);
- test generator (combination wave generator, 10/700  $\mu$ s generator);
- decoupling network/protection devices;
- additional resistors, 10  $\Omega$  and 40  $\Omega$  (see B.1 of annex B).

### 7.2 Test set-up for tests applied to EUT power supply

The surge is to be applied to the EUT power supply terminals via the capacitive coupling network (see figures 6, 7, 8 and 9). Decoupling networks are required in order to avoid possible adverse effects on equipment not under test that may be powered by the same lines and to provide sufficient decoupling impedance to the surge wave so that the specified wave may be developed on the lines under test.

If not otherwise specified the power cord between the EUT and the coupling/decoupling network shall be 2 m in length (or shorter).

To simulate the representative coupling impedances, in some cases additional specified resistors have to be used for the tests (explanations, see B.1 of annex B).

NOTE In some countries (e.g. USA) standards for a.c. lines require the tests according to figures 7 and 9 with a 2  $\Omega$  impedance although this is a more severe test. The general requirement is 10  $\Omega$ .

### 7.3 Test set-up for tests applied to unshielded unsymmetrically operated interconnection lines

In general, the surge is applied to the lines in accordance with figure 10 via capacitive coupling. The coupling/decoupling network shall not influence the specified functional conditions of the circuits to be tested.

An alternative test set-up (coupling via arrestors) is given in figure 11 for circuits with a higher signal transfer rate. Selection shall be made depending on the capacitive load with respect to the transmission frequency.

If not otherwise specified, the interconnection line between the EUT and the coupling/decoupling network shall be 2 m in length (or shorter).

#### 7.4 Test set-up for tests applied to unshielded symmetrically operated interconnection/telecommunication lines (figure 12)

For balanced interconnection/telecommunication circuits, the capacitive coupling method can normally not be used. In this case, the coupling is performed via gas arrestors (CCITT Recommendation K.17). Test levels below the ignition point of the coupling arrestor (about 300 V for a 90 V arrestor) cannot be specified (except in the case of secondary protection without gas arrestors).

NOTE Two test configurations are to be considered:

- for the equipment level immunity test with only secondary protection at the EUT at a low test level, e.g. 0,5 kV or 1 kV,
- for the system level immunity test with additional primary protection at a higher test level, e.g. 2 kV or 4 kV.

If not otherwise specified the interconnection line between the EUT and the coupling/decoupling network shall be 2 m in length (or shorter).

#### 7.5 Test set-up for tests applied to shielded lines

In the case of shielded lines a coupling/decoupling network may not be applicable.

Thus the surge is applied to the shields (metallic enclosures) of the EUTs and connected shields of the lines in accordance with figure 13. For shields connected at one end figure 14 applies. For decoupling the connected safety earthwire a safety isolating transformer shall be used. Normally, the maximum length of the specified shielded cable shall be used. With respect to the frequency spectrum of the surge 20 m length of the specified shielded cable shall be used in non-inductively bundled configuration for physical reasons.

Rules for application of the surge to shielded lines:

a) *Shields earthed at both ends*

- the surge injection on the shield shall be carried out according to figure 13.

b) *Shields earthed at one end*

- the test shall be carried out according to figure 14. The capacitor C represents the cable capacity to earth and the value may be calculated with 100 pF/m. As a representative value 10 nF may be used unless otherwise specified.

The test level applied on shields is the "line-to-earth value" ( $2 \Omega$  impedance).

#### 7.6 Test set-up to apply potential differences

If it is necessary to apply potential differences which simulate voltages that can occur within a system, the tests may be carried out in accordance with figure 13 for systems with shielded lines, shields earthed at both ends, and in accordance with figure 14 for systems with unshielded lines or shielded lines earthed only at one end.

## 7.7 Other test set-ups

If one of the specified coupling methods in the test set-up cannot be used for functional reasons, alternative methods (suitable for the special case) shall be specified in the dedicated product standard.

## 7.8 Test conditions

The operational test conditions and the installation conditions shall be in accordance with the product specification and shall include the:

- test configuration (hardware);
- test procedure (software).

## 8 Test procedure

### 8.1 Laboratory reference conditions

In order to minimize the impact of environmental parameters on test results, the test shall be carried out in climatic and electromagnetic reference conditions as specified in 8.1.1 and 8.1.2.

#### 8.1.1 Climatic conditions

Unless otherwise specified by the committee responsible for the generic or product standard, the climatic conditions in the laboratory shall be within any limits specified for the operation of the EUT and the test equipment by their respective manufacturers.

Tests shall not be performed if the relative humidity is so high as to cause condensation on the EUT or the test equipment.

NOTE Where it is considered that there is sufficient evidence to demonstrate that the effects of the phenomenon covered by this standard are influenced by climatic conditions, this should be brought to the attention of the committee responsible for this standard.

#### 8.1.2 Electromagnetic conditions

The electromagnetic environment of the laboratory shall not influence the test results.

### 8.2 Application of the surge in the laboratory

The characteristics and performance of the test generators shall be as specified in 6.1.1 and 6.2.1; the calibration of the generators shall be performed according to 6.1.2 and 6.2.2.

The test shall be performed according to the test plan that shall specify (see also B.2 of annex B) the test set-up with

- generator and other equipment utilized;
- test level (voltage/current) (see annex A);
- generator source impedance;
- polarity of the surge;
- internal or external generator trigger;
- number of tests: at least five positive and five negative at the selected points;

- repetition rate: maximum 1/min.

NOTE Most protectors in common use have low average power capabilities, even though their peak power or peak energy handling can deal with high currents. Therefore the maximum repetition rate (the time between two surges and the recovery time) depends on the built-in protection devices of the EUT.

- inputs and outputs to be tested;

NOTE In the case of several identical circuits representative measurements on a selected number of circuits may be sufficient.

- representative operating conditions of the EUT;
- sequence of application of the surge to the circuits;
- phase angle in the case of a.c. power supply;
- actual installation conditions, for example:

AC: neutral earthed,

DC: (+) or (–) earthed to simulate the actual earthing conditions

Information on the mode to perform the tests is given in B.2 of annex B.

If not otherwise specified the surges have to be applied synchronized to the voltage phase at the zero-crossing and the peak value of the a.c. voltage wave (positive and negative).

The surges have to be applied line to line and line(s) and earth. When testing line to earth the test voltage has to be applied successively between each of the lines and earth, if there is no other specification.

NOTE When using the combination wave generator to test two or more lines (telecommunication lines) to earth the duration of the test pulse might be reduced.

The test procedure shall also consider the non-linear current-voltage characteristics of the equipment under test. Therefore the test voltage has to be increased by steps up to the test level specified in the product standard or test plan.

All lower levels including the selected test level shall be satisfied. For testing the secondary protection, the output voltage of the generator shall be increased up to the worst-case voltage breakdown level (let-through level) of the primary protection.

If the actual operating signal sources are not available, they may be simulated. Under no circumstances may the test level exceed the product specification. The test shall be carried out according to a test plan.

To find all critical points of the duty cycle of the equipment, a sufficient number of positive and negative test pulses shall be applied. For acceptance test a previously unstressed equipment shall be used or the protection devices shall be replaced.

## 9 Evaluation of test results

The test results shall be classified in terms of the loss of function or degradation of performance of the equipment under test, relative to a performance level defined by its manufacturer or the requestor of the test, or agreed between the manufacturer and the purchaser of the product. The recommended classification is as follows:

- a) normal performance within limits specified by the manufacturer, requestor or purchaser;
- b) temporary loss of function or degradation of performance which ceases after the disturbance ceases, and from which the equipment under test recovers its normal performance, without operator intervention;
- c) temporary loss of function or degradation of performance, the correction of which requires operator intervention;
- d) loss of function or degradation of performance which is not recoverable, owing to damage to hardware or software, or loss of data.

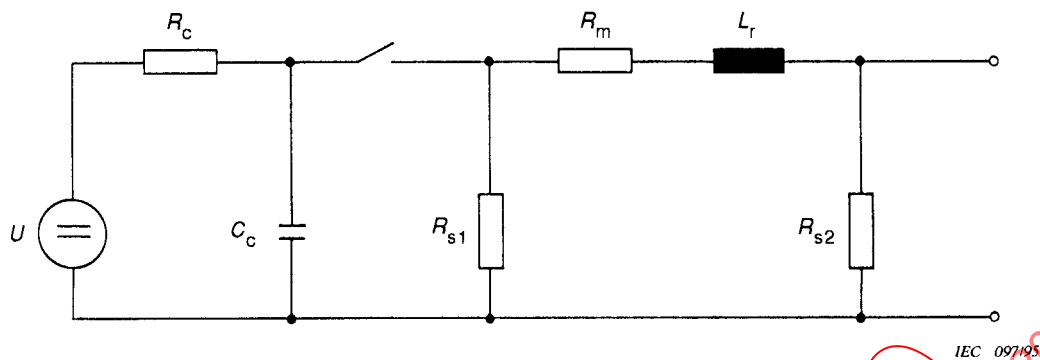
The manufacturer's specification may define effects on the EUT which may be considered insignificant, and therefore acceptable.

This classification may be used as a guide in formulating performance criteria, by committees responsible for generic, product and product-family standards, or as a framework for the agreement on performance criteria between the manufacturer and the purchaser, for example where no suitable generic, product or product-family standard exists.

## 10 Test report

The test report shall contain all the information necessary to reproduce the test. In particular, the following shall be recorded:

- the items specified in the test plan required by clause 8 of this standard;
- identification of the EUT and any associated equipment, for example, brand name, product type, serial number;
- identification of the test equipment, for example, brand name, product type, serial number;
- any special environmental conditions in which the test was performed, for example, shielded enclosure;
- any specific conditions necessary to enable the test to be performed;
- performance level defined by the manufacturer, requestor or purchaser;
- performance criterion specified in the generic, product or product-family standard;
- any effects on the EUT observed during or after the application of the test disturbance, and the duration for which these effects persist;
- the rationale for the pass/fail decision (based on the performance criterion specified in the generic, product or product-family standard, or agreed between the manufacturer and the purchaser);
- any specific conditions of use, for example cable length or type, shielding or grounding, or EUT operating conditions, which are required to achieve compliance.

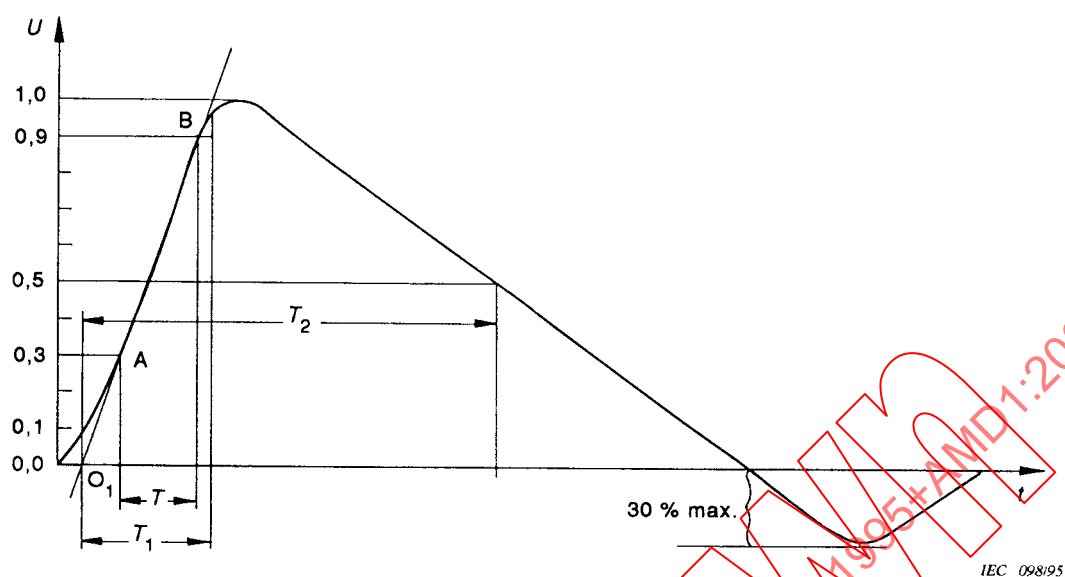


- $U$  High-voltage source  
 $R_c$  Charging resistor  
 $C_c$  Energy storage capacitor  
 $R_s$  Pulse duration shaping resistor  
 $R_m$  Impedance matching resistor  
 $L_r$  Rise time shaping inductor

Figure 1 – Simplified circuit diagram of the combination wave generator

Table 2 – Definitions of the waveform parameters 1,2/50  $\mu$ s

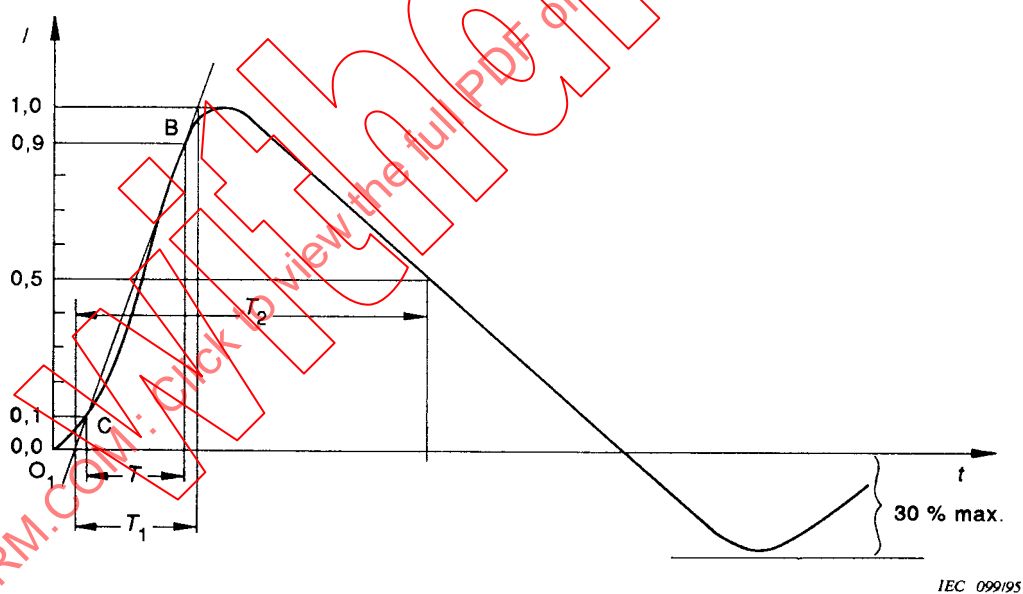
Definitions	In accordance with IEC 60060-1		In accordance with IEC 60469-1	
	Front time	Time to half value	Rise time (10 % - 90 %)	Duration time (50 % - 50 %)
	$\mu$ s	$\mu$ s	$\mu$ s	$\mu$ s
Open-circuit voltage	1,2	50	1	50
Short-circuit current	8	20	6,4	16
NOTE In existing IEC publications the waveforms 1,2/50 $\mu$ s and 8/20 $\mu$ s are generally defined according to IEC 60060-1 as shown in figures 2 and 3. Other IEC recommendations are based on waveform definitions according to IEC 60469-1 as shown in table 2.				
Both definitions are valid for this section of IEC 61000-4 and describe just one single generator.				



Front time:  $T_1 = 1,67 \times T = 1,2 \mu\text{s} \pm 30 \%$

Time to half-value:  $T_2 = 50 \mu\text{s} \pm 20 \%$

**Figure 2 – Waveform of open-circuit voltage (1,2/50  $\mu\text{s}$ )**  
(waveform definition according to IEC 60060-1)

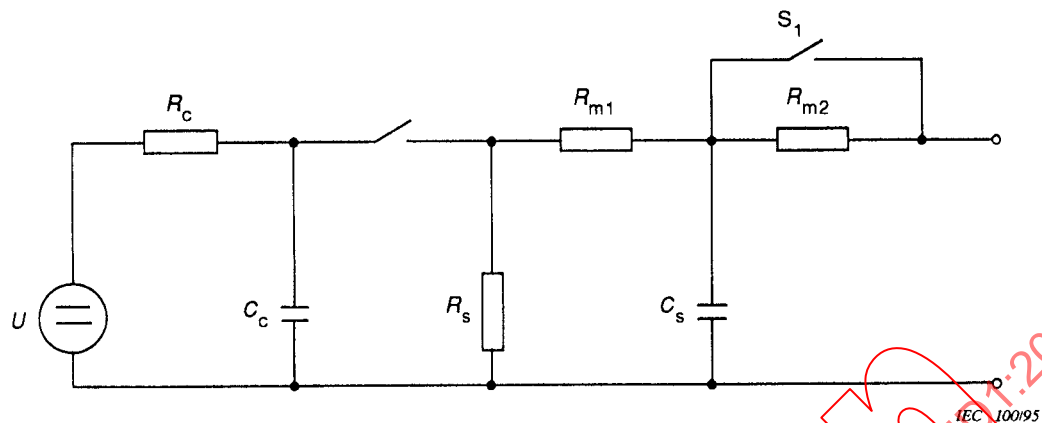


Front time:  $T_1 = 1,25 \times T = 8 \mu\text{s} \pm 20 \%$

Time to half-value:  $T_2 = 20 \mu\text{s} \pm 20 \%$

**Figure 3 – Waveform of short-circuit current (8/20  $\mu\text{s}$ )**  
(waveform definition according to IEC 60060-1)



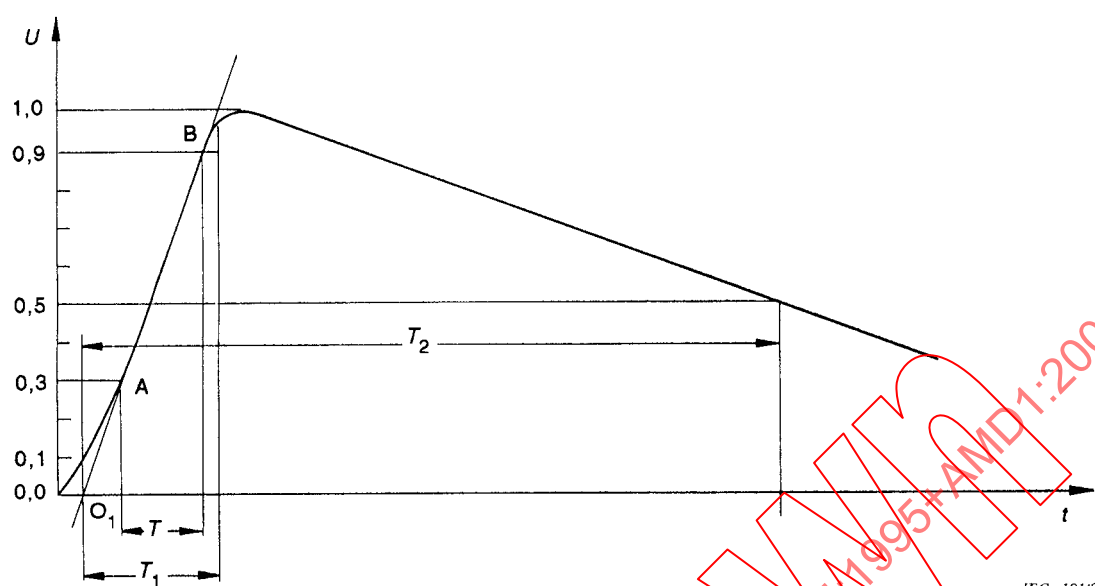


- $U$  High-voltage source  
 $R_c$  Charging resistor  
 $C_c$  Energy storage capacitor (20  $\mu\text{F}$ )  
 $R_s$  Pulse duration shaping resistor (50  $\Omega$ )  
 $R_m$  Impedance matching resistors ( $R_{m1} = 15 \Omega$ ;  $R_{m2} = 25 \Omega$ )  
 $C_s$  Rise time shaping capacitor (0,2  $\mu\text{F}$ )  
 $S_1$  Switch closed when using external matching resistors

**Figure 4 – Simplified circuit diagram of the 10/700  $\mu\text{s}$  impulse generator (according to CCITT, Blue book Vol. IX, figure 1/K.17)**

**Table 3 – Definitions of the waveform parameters 10/700  $\mu\text{s}$**

Definitions	In accordance with CCITT, Blue book, Vol. IX		In accordance with IEC 60469-1	
	Front time $\mu\text{s}$	Time to half-value $\mu\text{s}$	Rise time (10 % - 90 %) $\mu\text{s}$	Duration time (50 % - 50 %) $\mu\text{s}$
Open-circuit voltage	10	700	6,5	700
Short-circuit current	–	–	4	300
NOTE In existing IEC and CCITT publications, the waveform 10/700 $\mu\text{s}$ is generally defined according to IEC 60060-1 as shown in figure 5. Other IEC recommendations are based on waveform definitions according to IEC 60469-1 as shown in table 3.				
Both definitions are valid for this section of IEC 61000-4 and describe just one single generator.				



IEC 101/95

Front time:  $T_1 = 1,67 \times T = 10 \mu s \pm 30 \%$

Time to half-value:  $T_2 = 700 \mu s \pm 20 \%$

**Figure 5 – Waveform of open-circuit voltage (10/700  $\mu s$ )  
(waveform definition according to CCITT)**

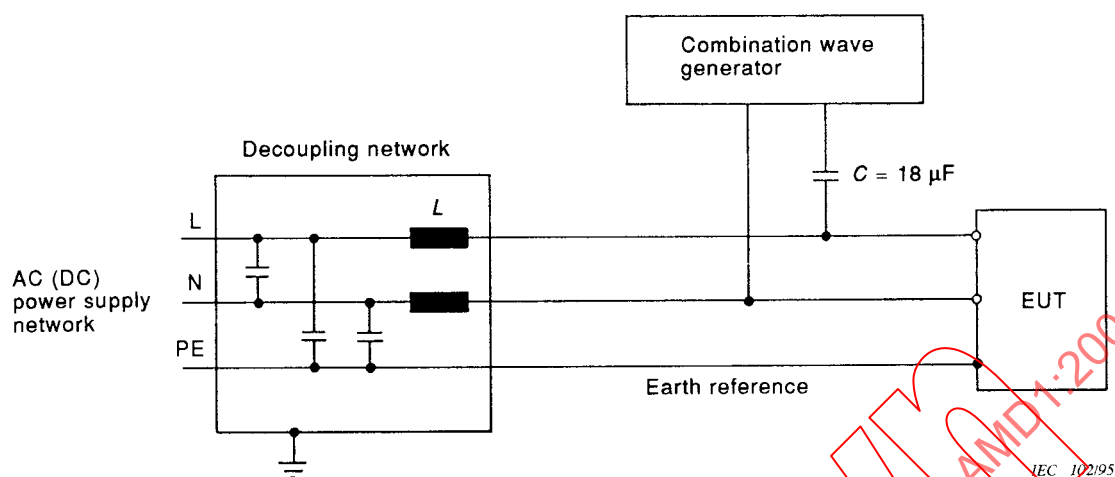


Figure 6 – Example of test set-up for capacitive coupling on a.c./d.c. lines; line-to-line coupling (according to 7.2)

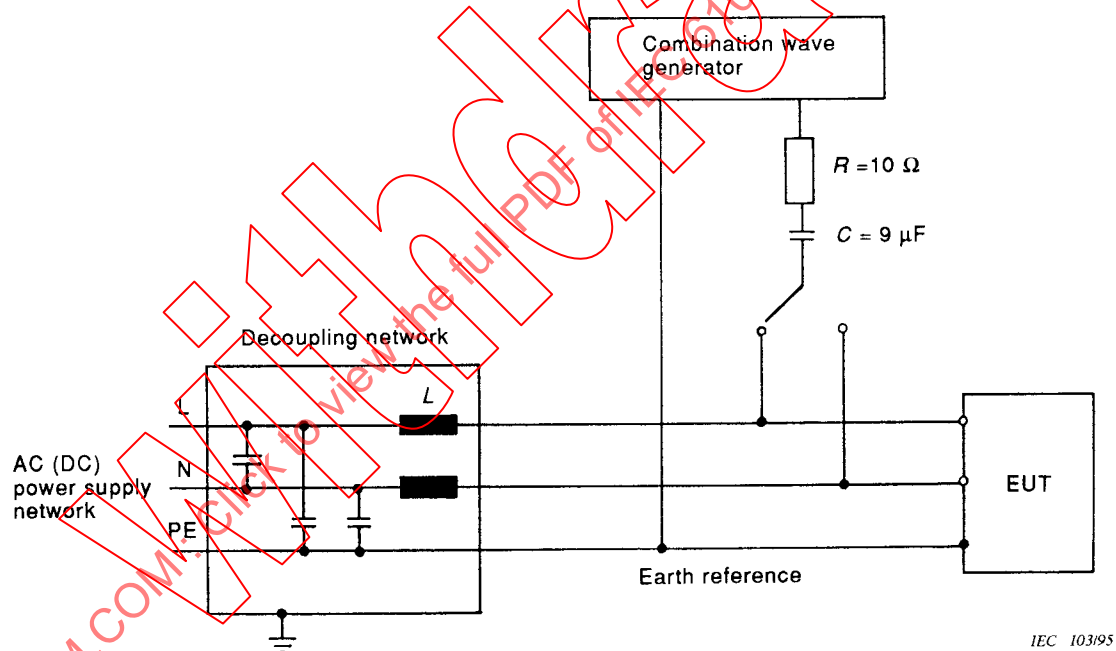


Figure 7 – Example of test set-up for capacitive coupling on a.c./d.c. lines; line-to-earth coupling (according to 7.2)

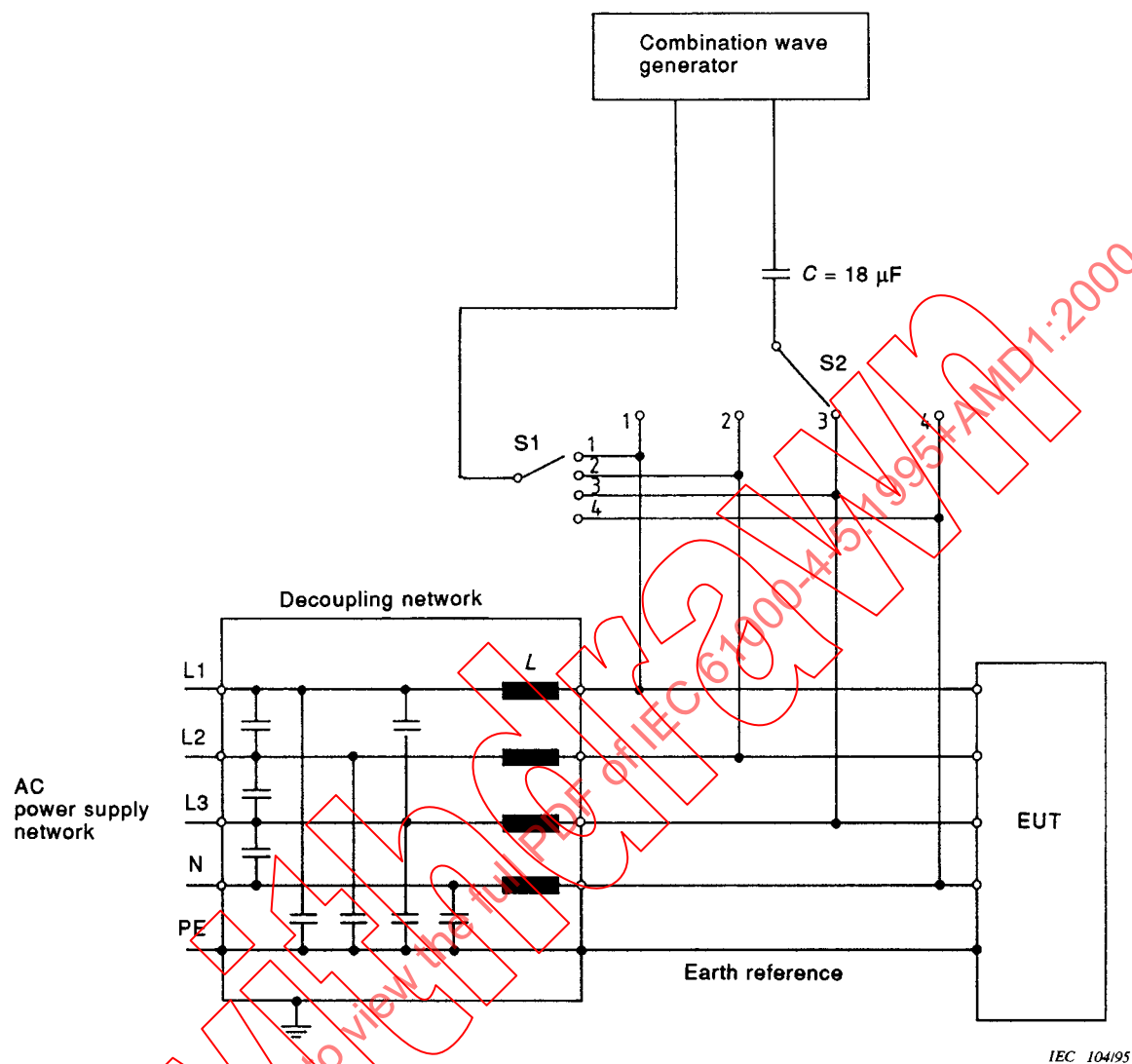
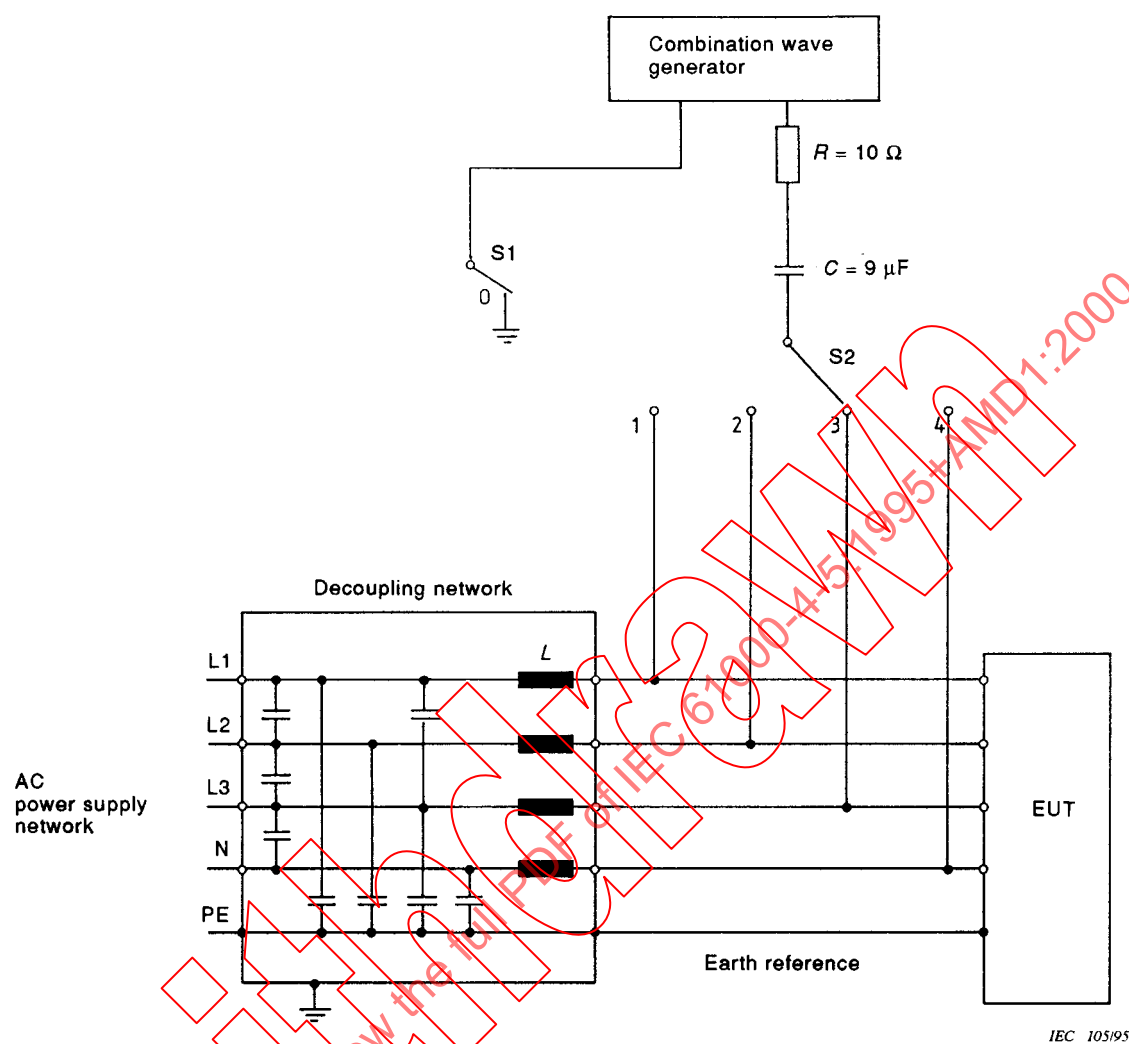
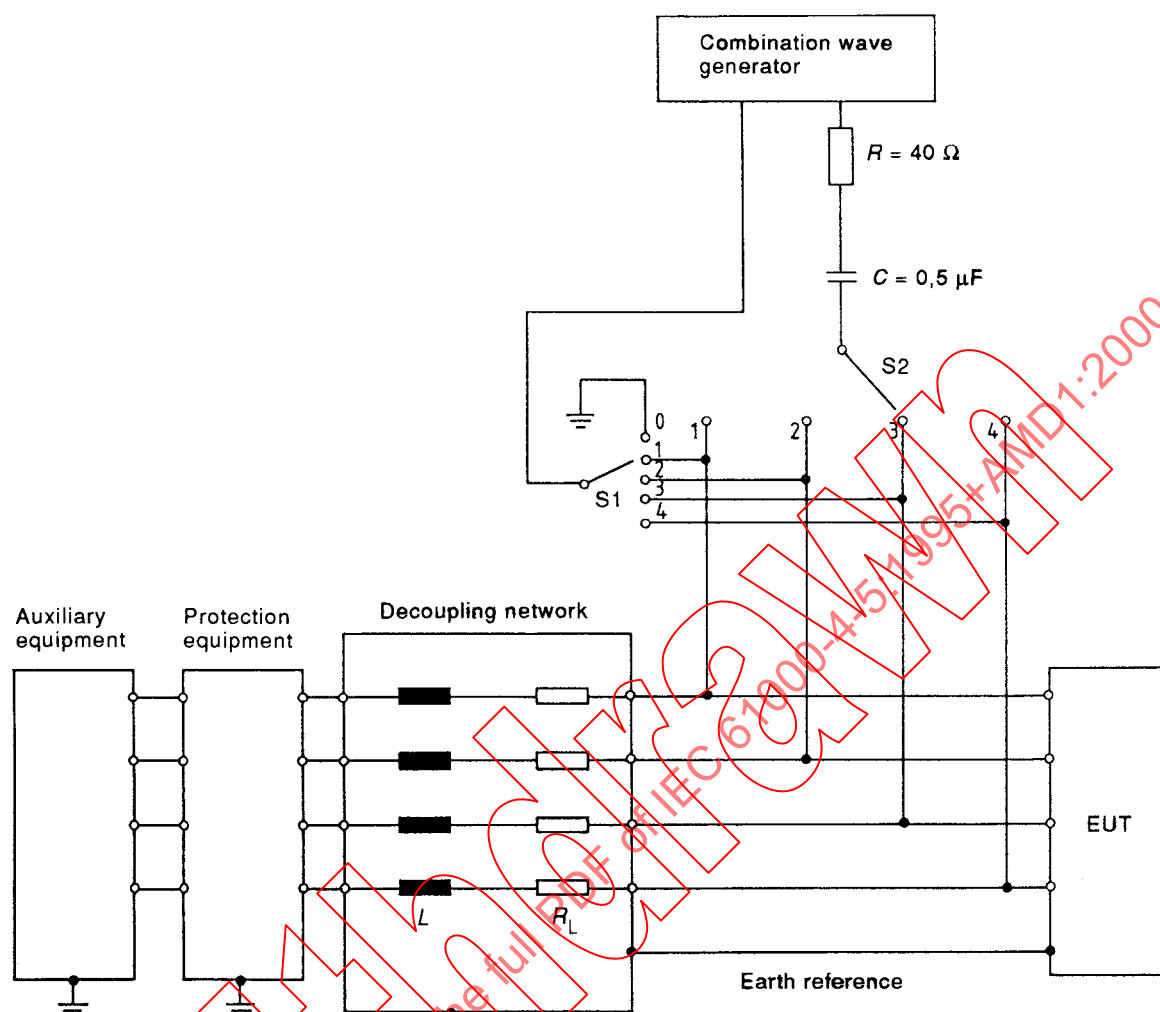


Figure 8 – Example of test set-up for capacitive coupling on a.c. lines (3 phases); line L3 to line L1 coupling (according to 7.2)



- 1) Switch  $S1$ 
  - line to earth: position 0
- 2) Switch  $S2$ 
  - during test positions 1 to 4

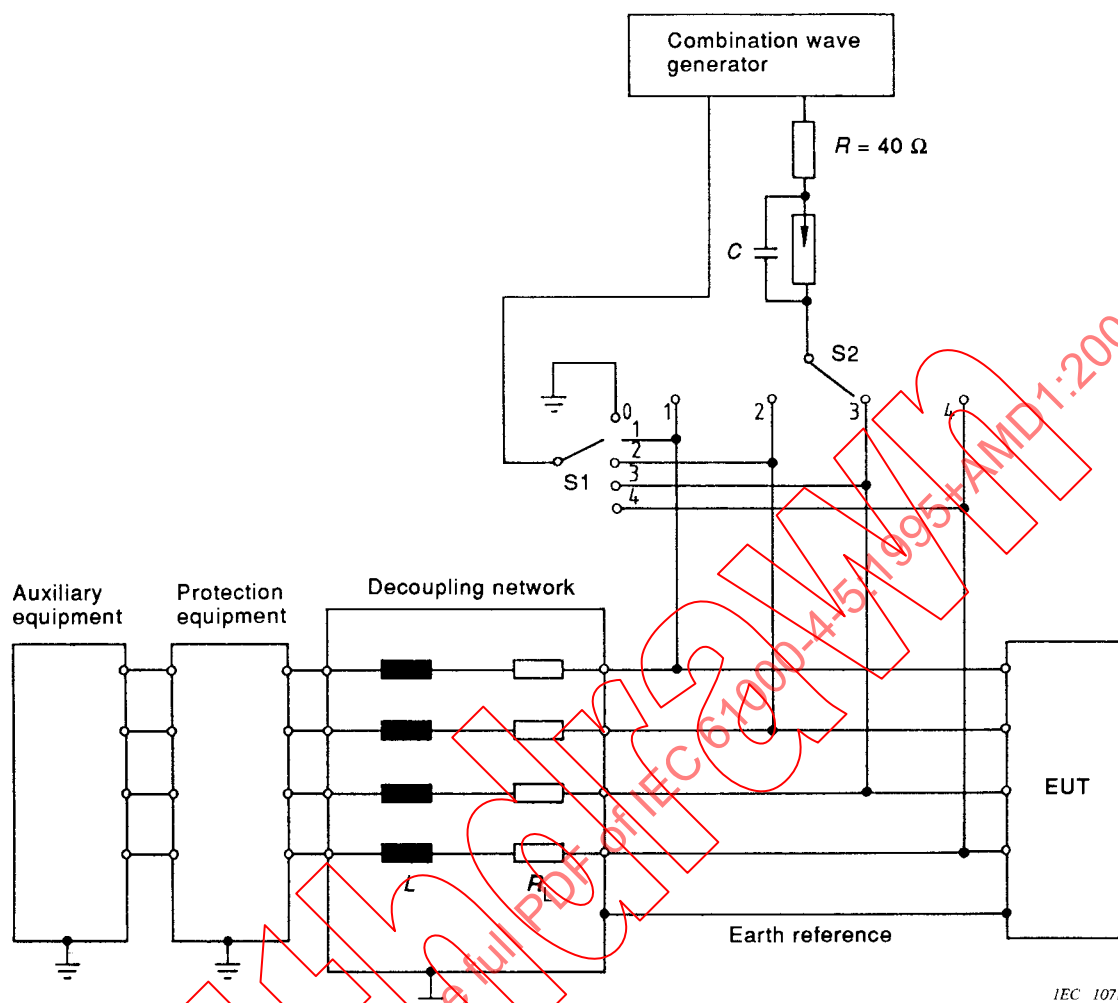
**Figure 9 – Example of test set-up for capacitive coupling on a.c. lines (3 phases); line L3 to earth coupling (according to 7.2); generator output earthed**



IEC 106/95

- 1) Switch  $S1$ 
  - line to earth: position 0
  - line to line: positions 1 to 4
- 2) Switch  $S2$ 
  - during the test positions 1 to 4, but not in the same position with switch  $S1$
- 3)  $L = 20 \, \text{mH}$ ,  $R_L$  represents the resistive part of  $L$

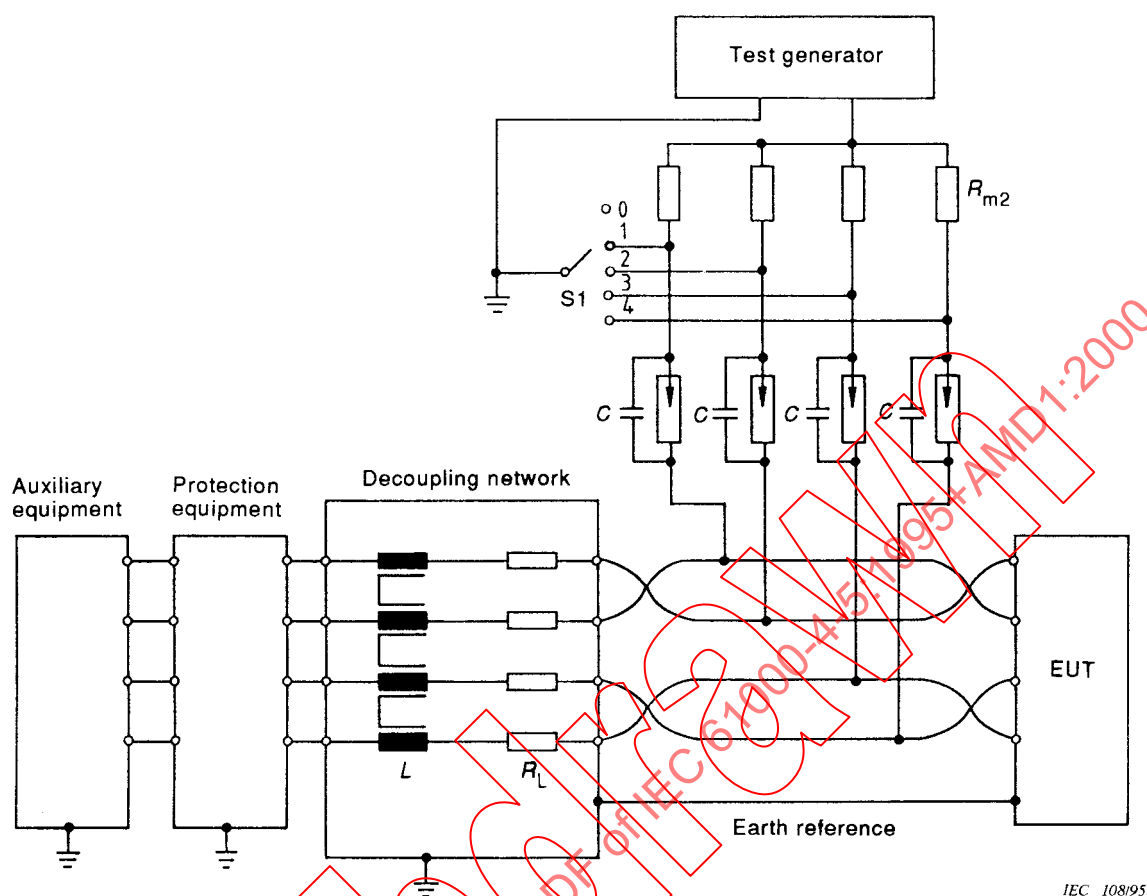
**Figure 10 – Example of test set-up for unshielded interconnection lines; line-to-line/line-to-earth coupling (according to 7.3), coupling via capacitors**



IEC 107/95

- 1) Switch S1
  - line to earth: position 0
  - line to line: positions 1 to 4
- 2) Switch S2
  - during the test positions 1 to 4, but not in the same position with switch S1
- 3)  $L = 20 \text{ mH}$ ,  $R_L$  represents the resistive part of  $L$

**Figure 11 – Example of test set-up for unshielded unsymmetrically operated lines; line-to-line/line-to-earth coupling (according to 7.3), coupling via arrestors**



IEC 108/95

- a) Switch  $S1$ 
  - line to earth: position 0
  - line to line: positions 1 to 4 (line in turn earthed)
- b) Calculation of  $R_{m2}$  when using CWG (1,2/50  $\mu s$  generator)
 

Example for  $n = 4$ :

$$R_{m2} = 4 \times 40 \, \Omega = 160, \text{ max. } 250 \, \Omega$$

Calculation of  $R_{m2}$  when using 10/700  $\mu s$  generator)

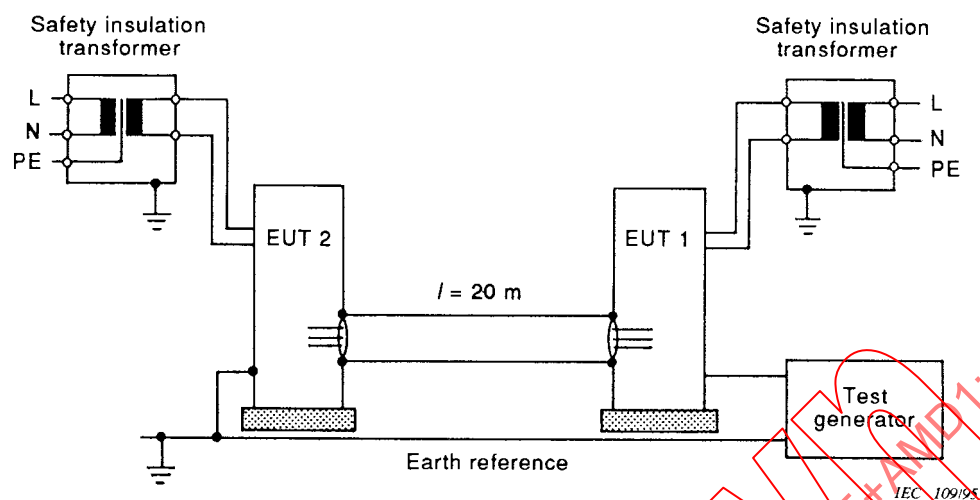
The internal matching resistor  $R_{m2}$  (25  $\Omega$ ) is replaced by external  $R_{m2} = n \times 25 \, \Omega$  per conductor. (for  $n$  conductors with  $n$  equal or greater than 2).

Example for  $n = 4$ :

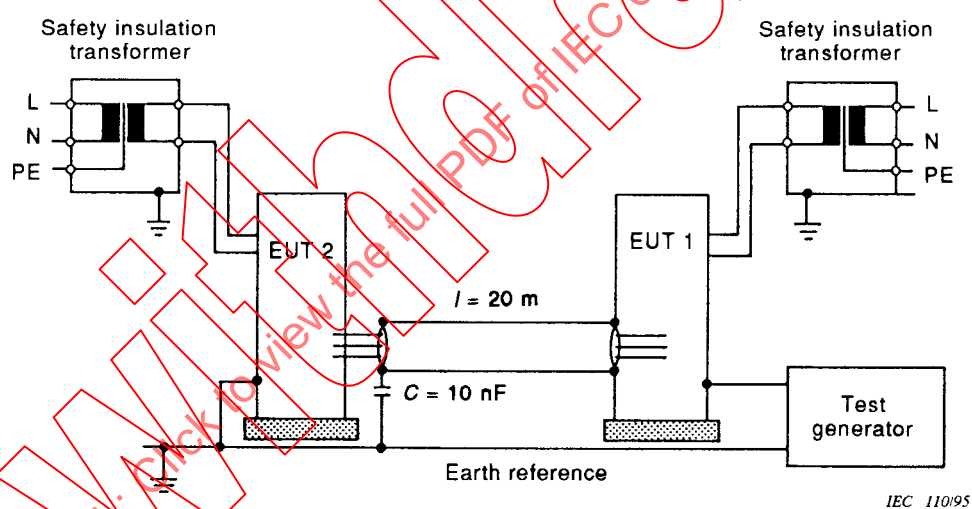
$$R_{m2} = 4 \times 25 \, \Omega = 100 \, \Omega, R_{m2} \text{ shall not exceed } 250 \, \Omega$$
- c)  $C = 0,1 \, \mu F$  for frequencies of the transmission signal below 5 kHz;  
at higher frequencies no capacitors are used
- d)  $L = 20 \, mH$ ,  $R_L$ : value depending on negligible attenuation of the transmission signal

**Figure 12 – Example of test set-up for unshielded symmetrically operated lines (telecommunication lines); line-to-line/line-to-earth coupling (according to 7.4), coupling via arrestors**





**Figure 13 – Example of test set-up for tests applied to shielded lines (according to 7.5) and to apply potential differences (according to 7.6), conductive coupling**



**Figure 14 – Example of test set-up for tests applied to unshielded lines and shielded lines earthed only at one end (according to 7.5) and to apply potential differences (according to 7.6), conductive coupling**

## **Annex A** (normative)

### **Selection of generators and test levels**

The selection of the test levels shall be based on the installation conditions. For this purpose table A.1 should be used, together with information and examples given in B.3 of annex B where:

- Class 0: Well-protected electrical environment, often within a special room.
- Class 1: Partly protected electrical environment.
- Class 2: Electrical environment where the cables are well separated, even at short runs.
- Class 3: Electrical environment where cables run in parallel.
- Class 4: Electrical environment where the interconnections are running as outdoor cables along with power cables, and cables are used for both electronic and electric circuits.
- Class 5: Electrical environment for electronic equipment connected to telecommunication cables and overhead power lines in a non-densely populated area.
- Class x: Special conditions specified in the product specification.

Additional information is given in figures B.1 to B.3 of annex B.

To demonstrate the system level immunity, additional measures relevant to the actual installation conditions, e.g. primary protection, should be taken.

**Table A.1 – Selection of the test levels (depending on the installation conditions)**

Installation class	Test levels							
	Power supply Coupling mode		Unbalanced operated circuits/lines, LDB Coupling mode		Balanced operated circuits/lines Coupling mode		SDB, DB <sup>1)</sup> Coupling mode	
	Line to line kV	Line to earth kV	Line to line kV	Line to earth kV	Line to line kV	Line to earth kV	Line to line kV	Line to earth kV
0	NA	NA	NA	NA	NA	NA	NA	NA
1	NA	0,5	NA	0,5	NA	0,5	NA	NA
2	0,5	1,0	0,5	1,0	NA	1,0	NA	0,5
3	1,0	2,0	1,0	2,0 <sup>3)</sup>	NA	2,0 <sup>3)</sup>	NA	NA
4	2,0	4,0 <sup>3)</sup>	2,0	4,0 <sup>3)</sup>	NA	2,0 <sup>3)</sup>	NA	NA
5	2) <sup>2)</sup>	2) <sup>2)</sup>	2,0	4,0 <sup>3)</sup>	NA	4,0 <sup>3)</sup>	NA	NA
x								
<sup>1)</sup> Limited distance, special configuration, special layout, 10 m to max. 30 m: no test is advised at interconnection cables up to 10 m, only class 2 is applicable. <sup>2)</sup> Depends on the class of the local power supply system. <sup>3)</sup> Normally tested with primary protection.								
Explanation: DB = data bus (data line) SDB = short-distance bus LDB = long-distance bus NA = not applicable								

The surges (and test generators) related to the different classes are as in the following:

Classes 1 to 4: 1,2/50 µs (8/20 µs).

Class 5: 1,2/50 µs (8/20 µs) for ports of power lines and short-distance signal circuits/lines.

10/700 µs for ports of long-distance signal circuits/lines.

The source impedances shall be as indicated in the figures of the test set-ups concerned.

## **Annex B** (informative)

### **Explanatory notes**

#### **B.1 Different source impedances**

The selection of the source impedance of the generator depends on:

- the kind of cable/conductor/line (a.c. power supply, d.c. power supply, interconnection, etc.);
- the length of the cables/lines;
- indoor/outdoor conditions;
- application of the test voltage (line to line or lines to earth).

The impedance of  $2\ \Omega$  represents the source impedance of the low-voltage power supply network. The generator with its effective output impedance of  $2\ \Omega$  is used.

The impedance of  $12\ \Omega$  ( $10\ \Omega + 2\ \Omega$ ) represents the source impedance of the low-voltage power supply network and earth.

The generator with an additional resistor of  $10\ \Omega$  in series is used.

The impedance of  $42\ \Omega$  ( $40\ \Omega + 2\ \Omega$ ) represents the source impedance between all other lines and earth.

The generator with an additional resistor of  $40\ \Omega$  in series is used.

In some countries (for instance, USA) standards for a.c. lines require the tests according to figures 7 and 9 with a  $2\ \Omega$  impedance; this is a more severe test. The general requirement is  $10\ \Omega$ .

#### **B.2 Application of the tests**

Two different kinds of tests are to be distinguished: at equipment level and at system level.

##### **B.2.1 Equipment level immunity**

The test shall be carried out in the laboratory on a single EUT. The immunity of the EUT thus tested is referred to equipment level immunity.

The test voltage shall not exceed the specified capability of the insulation to withstand high-voltage stress.

##### **B.2.2 System level immunity**

The test carried out in the laboratory refers to the EUT. The equipment level immunity does not assure the immunity of a system in all cases. For that reason a test on system level is advised which simulates the real installation. The simulated installation comprises protective devices (arrestors, varistors, shielded lines, etc.) and the real length and type of the interconnection lines.